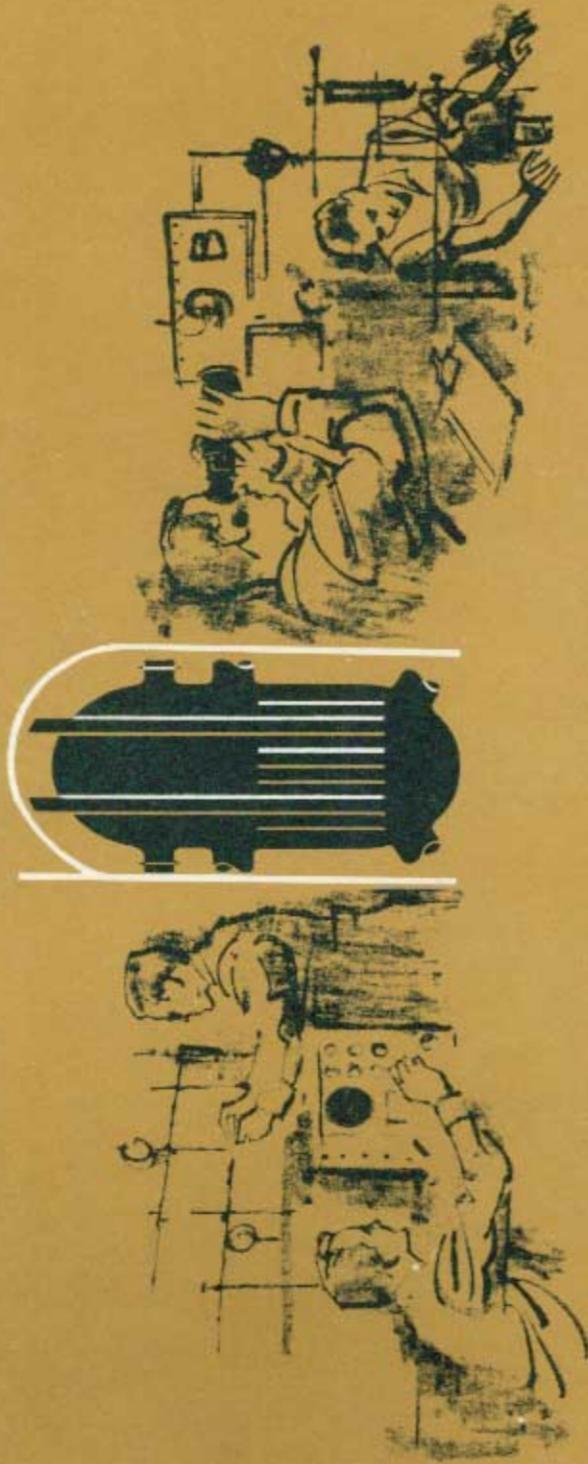


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Nuclear Materials and Equipment Corporation

Apollo, Pennsylvania 15613

U.S.A.

**COATING**

Monolayer
angular pa
CEMENTA
High density

SCRAP RE

Reprocessing
Recovery o

LABORATI

Instrumenta
Materials &
Radiochemi
Powder che

Corrosion &

Physical test
Hot Labora

DECONTA

Equipment
Clothing

RADIOPRE

Equipment
Architect-
Industrial st
Process de

CONSULTING SERVICE

Materials
Health Physics
Decontamination
Radiotriton application
Radioprocessing application
Personnel training

ARCHITECTURAL AND ENGINEERING SERVICE

Chemical processing facilities
Radiation processing facilities
Radioprocessing facilities

QUALITY CONTROL EQUIPMENT

Automatic weight, density and dimensional inspection
devices (Densitron®)
Crush strength apparatus
Surface area and density apparatus
Nuclear moisture-density gauges

CHEMICAL AND LABORATORY EQUIPMENT

Derivative polarographic instruments (Polaroscan®)
Constant potential coulometric titrator
Surface area and density apparatus
Pyro-hydrolysis tubes
Neutron irradiator-howitzer (Neutron Pac®)
Gamma irradiators

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Cathodic vacuum etchers
Vacuum evaporators
Combination vacuum etcher-evaporators
Remotized vacuum etcher and evaporators

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Melting and casing
Rolling
Pressing and compaction
Swaging
Extrusion
Vacuum annealing and out-gassing
Brazing and welding

FUEL MATERIALS

Bulk and fabricated
Uranium, plutonium and thorium
Metals, alloys and compounds

MODERATING MATERIALS

Beryllium oxide
Hydrides of zirconium, yttrium and niobium

CONTROL MATERIALS

Preparation and fabrication

RADIOACTIVE SOURCES

Isotopic heat sources
Neutron sources
Alpha sources

Beta and gamma sources

CRYSTAL BAR

Hafnium and zirconium

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Metal powders

Spherical metal powders

Brazing alloys

Powder metallurgy parts
Controlled porosity shapes

POWER GENERATORS

Radioisotopic thermoelectric generators
Thermionic converters

QUALITY CONTROL EQUIPMENT

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Crush strength apparatus

Surface area and density apparatus

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Gamma irradiators



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CONTENTS

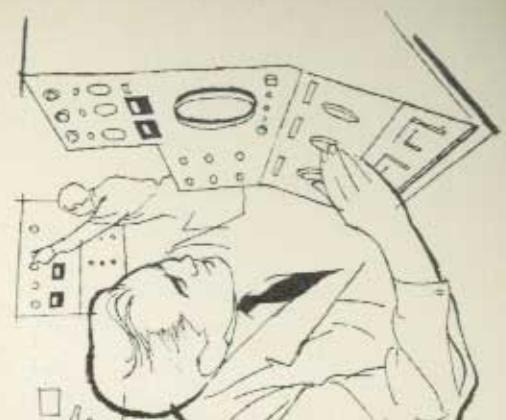
| PAGE | |
|------|---|
| 2 | Data Concerning the Elementary Particles |
| 3 | Alphabetical List of the Elements |
| 4 | Selected Properties of the Elements |
| 8 | Fission Reactions |
| | Breeding Processes |
| | Thermonuclear Reactions |
| 9 | Fission Fragments |
| 10 | Fundamental Physical Constants |
| | Prefixes for Units Adopted by NBS |
| 11 | Radioisotope Definitions |
| 12 | Methods of Radioisotope Production |
| 13 | Decay of a Radioelement |
| 14 | Exempt Quantities of Radioisotopes |
| 15 | Radioisotopes for Heat Sources |
| 16 | Thorium Materials Conversion Table |
| 17 | ThO_2 — % Theoretical Density and Equivalent g/cc |
| | Plutonium Materials Conversion Table |
| 18 | PuO_2 — % Theoretical Density and Equivalent g/cc |
| | Uranium Materials Conversion Table |
| 19 | UO_2 — % Theoretical Density and Equivalent g/cc |
| 20 | Base Charges for Enriched Uranium as UF_6 |
| | Base Charges for Depleted Uranium as UF_6 |
| | Use Charges for Special Nuclear Material |
| 21 | AEC Charges for Conversion of U_3O_8 to UF_6 |
| | AEC Withdrawal and Certification Charges for UF_6 |
| 22 | Loading Limits on AEC UF_6 Cylinders |
| 23 | AEC Charges for Contained Pu Isotopes — Pu-239 plus Pu-241 |
| 24 | Neutron Source Data |
| | Americium-241 |
| | Neptunium-237 |
| 25 | Tyler Standard Screen Scale Sieves |
| 26 | Energy Conversion Factors |
| 28 | Unit Conversion Charts |
| 31 | AEC Operations Offices |

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SERVICE



**DATA CONCERNING THE ELEMENTARY PARTICLES
THAT COMBINE TO BUILD UP ALL THE ATOMS
OF THE PERIODIC SYSTEM OF ELEMENTS**

| NAME AND SYMBOL | CHARGE | MASS | ENERGY | ATOMIC* WEIGHT | NUMBER | DIAMETER cm |
|---------------------|-------------------------------|------------------------------|----------------------------|----------------------------|----------------------------|--------------------------|
| Positive + | absolute | | mc^2 | relative | | |
| Negative - | | gram | | | | |
| Neutral O | e. s. u. | | ergs | $C^{12} = 12$ | one gram | |
| <hr/> | | | | | | |
| NEUTRON, η | O | 1.67470 $\times 10^{-24}$ | 1.5052 $\times 10^{-8}$ | 1.008661 | 5.9712 $\times 10^{23}$ | 2.8 $\times 10^{-13}$ |
| <hr/> | | | | | | |
| ELECTRON, β^- | - 4.8029 $\times 10^{-10}$ | 9.1083 $\times 10^{-25}$ | 8.186 $\times 10^{-7}$ | 5.4858 $\times 10^{-4}$ | 1.0979 $\times 10^{27}$ | 2.8 $\times 10^{-13}$ |
| <hr/> | | | | | | |
| PROTON, ρ | + 4.8029 $\times 10^{-10}$ | 1.67239 $\times 10^{-24}$ | 1.5031 $\times 10^{-8}$ | 1.007273 | 5.9795 $\times 10^{23}$ | 2.8 $\times 10^{-13}$ |
| <hr/> | | | | | | |
| POSITRON, β^+ | + 4.8029 $\times 10^{-10}$ | 9.1083 $\times 10^{-25}$ | 8.186 $\times 10^{-7}$ | 5.4858 $\times 10^{-4}$ | 1.0979 $\times 10^{27}$ | 2.8 $\times 10^{-13}$ |

*Atomic weights, as indicated in the Numec data section, are based upon $C^{12} = 12$.

**ALPHABETICAL LIST
OF THE ELEMENTS**

| At. No. | Name of Element | Sym. | At. Wt. | At. Na. | Name of Element | Sym. | At. Wt. | At. No. | Name of Element | Sym. | At. Wt. |
|------------|--------------------|------|------------|------------|--------------------|------|------------|------------|--------------------|------|------------|
| 89 | Actinium | Ac | 227 | 79 | Gold | Au | 196.967 | 59 | Praseodymium | Pr | 140.907 |
| 13 | Aluminum | Al | 26.9815 | 72 | Hafnium | Hf | 178.49 | 61 | Promethium | Pm | 14.5* |
| 95 | Americium | Am | 243* | 2 | Helium | He | 4.0026 | 91 | Protactinium | Pa | 231* |
| 51 | Antimony | Sb | 121.75 | 67 | Holmium | Ho | 164.930 | 88 | Radium | Ra | 226* |
| 18 | Argon | A | 39.948 | 1 | Hydrogen | H | 1.00797 | 86 | Radon | Rn | 222* |
| 33 | Arsenic | As | 74.9216 | 49 | Indium | In | 114.82 | 75 | Rhenium | Re | 186.2 |
| 85 | Astatine | At | 210* | 53 | Iodine | I | 126.9044 | 45 | Rhodium | Rh | 102.905 |
| 56 | Barium | Ba | 137.34 | 77 | Iridium | Ir | 192.2 | 37 | Rubidium | Rb | 85.47 |
| 97 | Berkelium | Bk | 247* | 26 | Iron | Fe | 55.847 | 44 | Ruthenium | Ru | 101.07 |
| 4 | Beryllium | Be | 9.0122 | 36 | Krypton | Kr | 83.80 | 62 | Samarium | Sm | 150.35 |
| 83 | Bismuth | Bi | 208.980 | 57 | Lanthanum | La | 138.91 | 21 | Scandium | Sc | 44.956 |
| 5 | Boron | B | 10.811 | 103 | Lawrencium | Lw | 257* | 34 | Selenium | Se | 78.96 |
| 35 | Bromine | Br | 79.909 | 82 | Lead | Pb | 207.19 | 14 | Silicon | Si | 28.086 |
| 48 | Cadmium | Cd | 112.40 | 3 | Lithium | Li | 6.939 | 47 | Silver | Ag | 107.870 |
| 20 | Calcium | Ca | 40.08 | 71 | Lutetium | Lu | 174.97 | 11 | Sodium | Na | 22.9898 |
| 98 | California | Cf | 249* | 25 | Manganese | Mn | 54.9380 | 38 | Strontium | Sr | 87.62 |
| 6 | Carbon | C | 12.01115 | 101 | Mendelevium | Md | 256* | 16 | Sulfur | S | 32.064 |
| 58 | Cerium | Ce | 140.12 | 80 | Mercury | Hg | 200.59 | 73 | Tantalum | Ta | 180.948 |
| 55 | Cesium | Cs | 132.905 | 42 | Molybdenum | Mo | 95.94 | 43 | Techneium | Tc | 99* |
| 17 | Chlorine | Cl | 35.453 | 60 | Neodymium | Nd | 144.24 | 52 | Tellurium | Te | 127.60 |
| 24 | Chromium | Cr | 51.996 | 10 | Neon | Ne | 20.183 | 65 | Terbium | Tb | 158.924 |
| 27 | Cobalt | Co | 58.9332 | 93 | Neptunium | Np | 237* | 81 | Thallium | Tl | 204.37 |
| 29 | Copper | Cu | 63.54 | 28 | Nickel | Ni | 58.71 | 90 | Thorium | Th | 232.038 |
| 96 | Curium | Cm | 248* | 41 | Niobium | Nb | 92.906 | 69 | Thulium | Tm | 168.934 |
| 66 | Dysprosium | Dy | 162.50 | 7 | Nitrogen | N | 14.0067 | 50 | Tin | Tn | 118.69 |
| 99 | Einsteinium | E | 254* | 102 | Nobelium | No | 254* | 22 | Titanium | Ti | 47.90 |
| 68 | Erbium | Er | 167.26 | 76 | Osmium | Os | 190.2 | 74 | Tungsten | W | 183.85 |
| 63 | Europium | Eu | 151.96 | 8 | Oxygen | O | 15.9994 | 92 | Uranium | U | 238.03 |
| 100 | Fermium | Fm | 253* | 46 | Palladium | Pd | 106.4 | 23 | Vanadium | V | 50.942 |
| 9 | Fluorine | F | 18.9984 | 15 | Phosphorus | P | 30.9738 | 54 | Xenon | Xe | 131.30 |
| 87 | Francium | Fr | 223* | 78 | Platinum | Pt | 195.09 | 70 | Ytterbium | Yb | 173.04 |
| 64 | Gadolinium | Gd | 157.25 | 94 | Plutonium | Pu | 242* | 39 | Yttrium | Y | 88.905 |
| 31 | Gallium | Ga | 69.72 | 84 | Polonium | Po | 209* | 30 | Zinc | Zn | 65.37 |
| 32 | Germanium | Ge | 72.59 | 19 | Potassium | K | 39.102 | 40 | Zirconium | Zr | 91.22 |

*Mass number of the most stable isotope.
**Atomic weights are based on C¹².

SELECTED PROPERTIES OF THE ELEMENTS

| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | Atom-ic No., Z |
|--------|----------------|---------|---|---------------------------------------|--|--------------------------------------|--------------------------------------|---------------------------------|--|---|------------------|------------------|----------------|----------------|
| PERIOD | Atom-ic No., Z | Sym-bol | Average thermal neutron absorption cross section barns* | Density @ 20°C except as noted g./cc. | Mod ulus of elas-ticity (ten-sion) $\times 10^6$ psi | Electri-cal resistiv-ity microhm/cm. | Latent heat of fusion cal./g. @ 20°C | Specific heat cal./g./°C @ 20°C | Coeffi-cient of linear thermal expan-sivity $\times 10^{-6}/^{\circ}\text{C}$ @ 20°C | Thermal conductivity cal./cm.-sec. @ 20°C | Melting point °C | Boiling point °C | Atom-ic No., Z | |
| 1 | 1 | H | 0.33 | .00008988 | | | 15.0 | 3.45 | | 4.061×10^{-4} | -259.4 | -252.5 | 1 | |
| | 2 | He | 0.007 | .0001785 | | | 104.2 | 1.25 | | 3.32×10^{-4} | >-272.2 | -268.6 | 2 | |
| 2 | 3 | Li | 71. | 0.534 | | 8.55(0°) | 0.79 | 56. | 0.17 | | 179. | *1317. | 3 | |
| | 4 | Be | 0.010 | 1.848 | 40.-44. | 4.0(20°) | .45 | 11.6 | .35 | | 1278. | ± 5 | 4 | |
| 2 | 5 | B | 755. | 2.34 | 64. | $1.8 \times 10^{12}(0^{\circ})$ | 0.309 | 8.3 | | 2300. | | 2970. | 5 | |
| | 6 | C | 0.0037 | 1.9-2.3 | 0.7 | 1375.(0°) | | 0.165 | 0.6-4.3 | 0.057 | 3550. | | 2550. | 5 |
| 2 | 7 | N | 1.9 | 0.0012506 | | | 6.2 | 0.247 | | 0.600×10^{-4} | -209.86 | -195.8 | 7 | |
| | 8 | O | <0.0002 | 0.001429 | | | 3.3 | 0.218 | | 0.590×10^{-4} | -218.4 | -183.07 | 8 | |
| 2 | 9 | F | 0.009 | 0.001696 | | | 10.1 | 0.18 | | | -219.62 | -188.14 | 9 | |
| | 10 | Ne | <1. | 0.00089990 | | | | | 1.1 $\times 10^{-4}$ | | -248.67 | -245.92 | 10 | |
| 3 | 11 | Na | 0.53 | 0.97126 | | 4.2(0°) | 27.5 | 295 | 71. | 0.32 | 97.81 ± 03 | 883. | 11 | |
| | 12 | Mg | 0.069 | 1.738 | 5.77 | 4.45(20°) | 89. | 0.245 | 26. | 0.38 | 651. | 1107. | 12 | |
| 3 | 13 | Al | 0.24 | 2.702 | 9.0 | 2.6548(20°) | 94.6 | 0.215 | 23.9 | 0.53 | 659.7 | 2057. | 13 | |
| | 14 | Si | 0.16 | 2.3325 | 1.6. | $10^3(0^{\circ})$ | 432. | 0.162 | 2.8-7.3 | 0.20 | 1410. | 2355. | 14 | |
| 3 | 15 | P | 0.20 | 2.07-1.93728 | | 107(11°) | 5.0 | 0.177 | 125. | | 44.1 ± 01 | 280. | 15 | |
| | 16 | S | 0.52 | 2.07 | | $2 \times 10^{23}(20^{\circ})$ | 9.3 | 0.175 | 64. | 6.31×10^{-4} | 112.8-119.0 | 444.6 | 16 | |
| 3 | 17 | Cl | 34. | 0.003214 | | | 21.6 | 0.116 | | 0.172×10^{-4} | -100.98 | -34.6 | 17 | |
| | 18 | A | 0.66 | 0.001784 | | | 6.7 | 0.125 | | 0.406×10^{-4} | -189.2 | -185.7 | 18 | |
| 4 | 19 | K | 2.1 | 0.862 | | 6.15(0°) | 14.5 | 0.177 | 83. | 0.24 | 63.65 | 774. | 19 | |
| | 20 | Ca | 0.44 | 1.55 | 3.2-3.8 | 3.91(0°) | 52.0 | 0.149 | 22. | 0.3 | 845. | ± 3 | 1487. | |
| 4 | 21 | Sc | 24. | 2.992 | | 61.0(22°) | 84.5 | 0.134 | | | 1539. | 2727. | 21 | |
| | 22 | Ti | 5.8 | 4.507 | 1.6.8 | 80.(0°) | 104.(est) | 0.124 | 8.41 | | 1675. | 3260. | 22 | |
| 4 | 23 | V | 5.00 | 6.01n.7 | 18.-20. | 24.8-26.0(20°) | 0.120 | 8.3 | | 0.074 | 1890. | ± 10 | 23 | |
| | 24 | Cr | 3.1 | 7.18-7.20 | 36. | 12.9(0°) | 96. | 0.11 | 6.2 | 0.16 | 1890. | | 2482. | |
| 4 | 25 | Mn | 13.2 | 7.24-7.44 | 23. | 185.(23°) | 64. | 0.115 | 22. | | 1244. | ± 3 | 2097. | |
| | 26 | Fe | 2.6 | 7.874 | 28.5 | 9.71(20°) | 65. | 0.11 | 11.7 | 0.18 | 1555. | | 2350. | |
| 4 | 27 | Co | 38. | 8.85 | 30. | 6.24(20°) | 58.4 | 0.099 | 13.8 | 0.165 | 1495. | | 2900. | |

*Thermal neutron absorption cross section (2200 m/s) barns
BNL-325, Second Edition and Supplement No. 1.

SELECTED PROPERTIES OF THE ELEMENTS

| | 11 | 12 | 13 | | | | | | | | | |
|------------------------------------|---------------------------------|---------------------------------|---------------|--|--|--|--|--|--|--|--|--|
| sl. vity, cm^2/sec | Melting point, $^\circ\text{C}$ | Boiling point, $^\circ\text{C}$ | Atomic No., Z | | | | | | | | | |
| 10^{-4} | -259.4 | -252.5 | 1 | | | | | | | | | |
| > -272.2 | -268.6 | 2 | | | | | | | | | | |
| 179. | $^{+1317.}$ | 3 | | | | | | | | | | |
| 1278. ± 5 | 2970. | 4 | | | | | | | | | | |
| 2300. | 2550. | 5 | | | | | | | | | | |
| 3550. | 4827. | 6 | | | | | | | | | | |
| 10^{-4} | -209.86 | -195.8 | 7 | | | | | | | | | |
| 10^{-4} | -218.4 | -183.07 | 8 | | | | | | | | | |
| -219.62 | -188.14 | 9 | | | | | | | | | | |
| 4 | -248.67 | -245.92 | 10 | | | | | | | | | |
| 97.81 ± 03 | 883. | 11 | | | | | | | | | | |
| 651. | 1107. | 12 | | | | | | | | | | |
| 6597 | 2057. | 13 | | | | | | | | | | |
| 1410. | 2355. | 14 | | | | | | | | | | |
| 44.1 ± 01 | 280. | 15 | | | | | | | | | | |
| $112.8 - 119.0$ | 444.6 | 16 | | | | | | | | | | |
| 0^{-4} | -100.98 | -34.6 | 17 | | | | | | | | | |
| 0^{-4} | -189.2 | -185.7 | 18 | | | | | | | | | |
| 63.65 | 774. | 19 | | | | | | | | | | |
| 845. ± 3 | 1487. | 20 | | | | | | | | | | |
| 0^{-4} | 2727. | 21 | | | | | | | | | | |
| 1675. | 3260. | 22 | | | | | | | | | | |
| 1890. ± 10 | $\div 3000.$ | 23 | | | | | | | | | | |
| 1890. | 2482. | 24 | | | | | | | | | | |
| 1244. ± 3 | 2097. | 25 | | | | | | | | | | |
| 1555. | 3500. | 26 | | | | | | | | | | |
| 1495. | 2900. | 27 | | | | | | | | | | |

| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 |
|-------------|----------------|--------|--|--|--------------------------------|-------------------------------------|---|---|--|--|---------------------------------|---------------------------------|----------------|
| P E R I O D | Atom-ic No., Z | Symbol | Average thermal neutron absorption cross section, barns* | Density @ 20°C except as noted | Modulus of elasticity, lb./in. | Electrical resistivity, microhm cm. | Latent heat of fusion, cal./g. 20°C | Specific heat, cal./g. 20°C | Coefficient of linear thermal expansivity $\times 10^{-8}/^\circ\text{C}$ 20°C | Thermal conductivity, cal./cm. $^2/\text{sec. } ^\circ\text{C}$ 20°C | Melting point, $^\circ\text{C}$ | Boiling point, $^\circ\text{C}$ | Atom-ic No., Z |
| Y | 28 | Ni | 4.6 | 8.902 ²¹ | 30. | 6.84(20°) | 74. | 0.105 | 13.3 | 0.22 | 1453. | 2732. | 28 |
| | 29 | Cu | 3.8 | 8.96 | 16. | 1.673(20°) | 50.6 | 0.092 | 16.5 | 0.94 | 1083.0 ± 0.1 | 2595. | 29 |
| | 30 | Zn | 1.1 | 7.133 ²² | 12. | 5.916(20°) | 24.09 | 0.0915 | 39.7 | 0.27 | 419.4 | 907. | 30 |
| Ga | 31 | Ga | 2.8 | 5.907 | | 17.4(20°) | 19.2 | 0.079 | 18. | 0.07-0.09 | 29.78 | 2403. | 31 |
| Ge | 32 | Ge | 2.5 | 5.323 ²³ | | 46 $\times 10^6$ (22°) | 0.073 | 5.75 | 0.14 | 937.4 | 814(at 36 atm) | 2830. | 32 |
| As | 33 | As | 4.3 | 5.727 ¹⁴ | | 33.3(20°) | 88.5 | 0.082 | 4.7 | 7.18 $\times 10^{-4}$ | 217. | 684.9 ± 1 | 33 |
| Se | 34 | Se | 12. | 4.79 | 8.4 | 12.0(0 ²) | 16.4 | 0.084 | 37. | | 7.2 | 58.78 | 34 |
| Br | 35 | Br | 6.7 | 3.12 | | 16.2 | 0.070 | | | 0.21 $\times 10^{-4}$ | -156.6 | -152.30 | 35 |
| Kr | 36 | Kr | 31 | 0.003743 | | 12.5(20°) | 6.5 | 0.080 | 90. | 38.89 | 688. | 36 | |
| Rb | 37 | Rb | 0.73 | 1.532 | | 23.1(20°) | 25. | 0.176 | | 769. | 1384. | 37 | |
| Sr | 38 | Sr | 1.2 | 2.60 | | 29.0(25°) | 46.0 | 0.071 | | 0.035 | 1495 ± 5 | 2927. | 38 |
| Y | 39 | Y | 1.3 | 4.45 | 17.0 | 40.0(20°) | 60 (est) | 0.066 | 5. | 0.211 | 1852 ± 2 | 3578. | 39 |
| Zr | 40 | Zr | 0.18 | 6.53 | 13.7 | 5.2(0°) | 69.0 | 0.065 | 7.1 | 0.125 | 2468 ± 10 | 4927. | 40 |
| Nb | 41 | Nb | 1.2 | 8.57 | 15.0 ²⁴ | 12.5(0°) | 70 (est) | 0.066 | 4.9 | 0.35 | 2610 | 5560. | 41 |
| Mo | 42 | Mo | 2.7 | 10.22 | 50. | 5.2(0°) | | | | 2200 ± 50 | | 42 | |
| Tc | 43 | Tc | 22. | 11.50 | | 7.6(0°) | | 0.057 | 9.1 | | 2250. | 3900. | 43 |
| Ru | 44 | Ru | 2.6 | 12.41 | 60. | 4.51(20°) | | 0.059 | 8.3 | 0.21 | 1960 ± 3 | 3727 ± 100 | 44 |
| Rh | 45 | Rh | 150. | 12.41 | 42. | 10.8(20°) | 34.2 | 0.058 | 11.8 | 0.17 | 1552. | 2927. | 45 |
| Pd | 46 | Pd | 8. | 12.02 | 17. | 1.59(20°) | 25. | 0.056 | 19.7 | 0.975 | 960.8 | 2212. | 46 |
| Ag | 47 | Ag | 63. | 10.50 ²⁰ | 11. | | | | | | | | 47 |
| Cd | 48 | Cd | 2450. | 8.65 | 8. | 6.83(0°) | 13.2 | 0.055 | 29.8 | 0.22 | 320.9 | 765. | 48 |
| In | 49 | In | 190. | 7.31 | | 8.37(20°) | 6.8 | 0.057 | 33. | 0.057 | 156.61 | 2000 ± 10 | 49 |
| Sn | 50 | Sn | .62 | 5.75 ¹¹ | 6. | 11.0(0°) | 14.5 | 0.054 | 23. | 0.16 | 231.89 | 2270. | 50 |
| Sb | 51 | Sb | 5.7 | 6.684 ²⁵ | 11.3 | 39.0 (0°) | 38.3 | 0.049 | 8.5-10.8 | 0.045 | 630.5 | 1380. | 51 |
| Te | 52 | Te | 4.7 | 6.24 | 6. | 4.36 $\times 10^3$ (25°) | 32.0 | 0.047 | 16.8 | 0.014 | 449.5 ± 0.3 | 989.8 ± 3.8 | 52 |

*Thermal neutron absorption cross section (2200 m⁻¹ s) barns
BNL-325, Second Edition and Supplement No. 1.

SELECTED PROPERTIES OF THE ELEMENTS

| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 |
|--------|--------------------------------|----------------|---|---|---|--|--|--|---|---|------------------------|------------------------|--------------------------------|
| PERIOD | Atom- ic No. <i>Z</i> | Sym- bol | Average thermal neutron absorption cross section burnt* | Density (g./20° C except as noted) | Mod- ulus of elas- ticity G/E × 10 ¹⁰ psi | Electrical resistivity microhm/cm. | Latent heat of fusion cal./g. 20° C | Specific heat cal./g. °C 20° C | Coeffi- cient of linear thermal expans- ivity × 10 ⁻⁴ /°C 20° C | Thermal conductivity cal./cm. ² cm./°C/sec 20° C | Melting point °C | Boiling point °C | Atom- ic No. <i>Z</i> |
| 1 | 53 | Xe | 7.0 35. | 4.93 0.005887 | 1.3 × 10 ¹⁵ (20°) | 14.2 | 0.052 | 93. | 10.4 × 10 ⁻⁴ | 113.5 | 184.35 | 53 | |
| 2 | 54 | | | | 20 (20°) | 3.8 | 0.048 | 97. | 1.24 × 10 ⁻⁴ | 111.9 | -107.1 ± 3 | 54 | |
| 3 | 55 | Cs | 28. | 1.873 3.51 | | | | | | 28.52 | 690. | 55 | |
| 4 | 56 | Ba | 1.2 | 5.98-6.186 | 5.70(25°) | 17.3 | 0.048 | 5.0 | 725. | 1140. | 56 | | |
| 5 | 57 | La | 8.9 | 6.67-8.23 | 75.0(25°) | 8.6 | 0.045 | 8. | 920. | 3469. | 57 | | |
| 6 | 58 | Ce | 0.73 | 6.782 | 68.1(25°) | 11.8 | 0.046 | 4. | 795. | 3468. | 58 | | |
| 7 | 59 | Pr | 1.13 | 6.80-7.004 | 64.0(25°) | 11.8 | 0.045 | 6. | 935. | 3127. | 59 | | |
| 8 | 60 | Nd | 46. | | | | | | 1024. | 3027. | 60 | | |
| 9 | 61 | Pm | | | | | | | | 1035. | 2730. | 61 | |
| 10 | 62 | Sm | 5600 | 7.536 | 8.0 | 88.(25°) | 0.043 | | | 1072. | 1900. | 62 | |
| 11 | 63 | Eu | 4300 | 5.259 | 90.0(25°) | 16.9 | 0.040 | 26. | | 826. | 1439. | 63 | |
| 12 | 64 | Gd | 46,000 | 7.9895 | 8-14 | 140.5(25°) | 16.4 | 0.071 | 4. | 1312. | ÷ 3000. | 64 | |
| 13 | 65 | Tb | 46 | 8.272 | | 23.6 | 0.044 | 7.0 | | 1356. ± 50 | 2800. | 65 | |
| 14 | 66 | Dy | 950 | 8.537 | 10-14 | 57.0(25°) | 26.4 | 0.041 | 9.0 | 0.024 | 1407. | 2600. | 66 |
| 15 | 67 | Ho | 65 | 8.803 | 11.0 | 87.0(25°) | | 0.039 | | | 146. | 2600. | 67 |
| 16 | 68 | Er | 173 | 9.051 | 107.0(25°) | 24.6 | 0.040 | 9.0 | 0.023 | 1497. | 2900. | 68 | |
| 17 | 69 | Tm | 127 | 9.332 | 79.0(25°) | 26.0 | 0.038 | | | 1545. | 1727. | 69 | |
| 18 | 70 | Yb | 37 | 6.977 | 29.0(25°) | 12.7 | 0.035 | 25. | | 824. ± 5 | 1427. | 70 | |
| 19 | 71 | Lu | 112 | 9.7872 | 79.0(25°) | 26.4 | 0.037 | | | | 1652. | 3327. | 71 |
| 20 | 72 | Hf | 105 | 13.29 | 20. | 35.1(25°) | 0.035 | 5.9 | | | 2150. | 5400. | 72 |
| 21 | 73 | Ta | 21 | 16.6 | 22. | 12.45(25°) | 38.0 | 0.034 | 6.5 | 0.13 | 2996. | 5425 ± 100 | 73 |
| 22 | 74 | W | 19.2 | 19.3 | 50. | 5.65(27°) | 44. | 0.032 | 4.6 | 0.397 | 3410. ± 20 | 5927. | 74 |
| 23 | 75 | Re | 86. | 21.02 | 66.7 | 19.3(20°) | 0.033 | 6.7 | .17 | 3180. | 5627. | 75 | |
| 24 | 76 | O ₆ | 15.3 | 22.57 | 80. | 9.5(20°) | 0.031 | 4.6 | | 3000. ± 10 | 5000. | 76 | |
| 25 | 77 | Ir | 440. | 22.42 ¹⁷ | 75. | 5.3(20°) | 0.031 | 6.8 | 0.14 | 2410. | 4572 ± 100 | 77 | |
| 26 | 78 | Pt | 8.8 | 21.45 | 21. | 10.6(20°) | 27. | 0.032 | 8.9 | 0.17 | 1769. | 3872 ± 100 | 78 |
| 27 | 79 | Au | 98.8 | 19.32 | 12. | 2.35(20°) | 16.1 | 0.031 | 14.2 | 0.71 | 1063. | 2966. | 79 |

*Thermal neutron absorption cross section (2200 m/s) barns
BNL-325, Second Edition and Supplement No. 1.

SELECTED PROPERTIES OF THE ELEMENTS

| 0 | 11 | 12 | 13 | Atom-ic No. Z | Melting point °C | Boiling point °C | Atomic activity cm. ⁻² ; sec. ⁻¹ °C |
|------------------|------------|------------|----|------------------|------------------|------------------|---|
| $\times 10^{-4}$ | 113.5 | 184.35 | 53 | 53 | 184.35 | 184.35 | $\times 10^{-4}$ |
| $\times 10^{-4}$ | 111.9 | -107.1 ± 3 | 54 | 54 | -107.1 ± 3 | 111.9 | $\times 10^{-4}$ |
| 28.52 | 690. | 55 | 55 | 55 | 690. | 55 | 28.52 |
| 725. | 1140. | 56 | 56 | 56 | 1140. | 56 | 725. |
| 33 | 920. | 57 | 57 | 57 | 3469. | 57 | 33 |
| 26 | 795. | 58 | 58 | 58 | 3468. | 58 | 26 |
| 28 | 935. | 59 | 59 | 59 | 3127. | 59 | 28 |
| 31 | 1024. | 60 | 60 | 60 | 3027. | 60 | 31 |
| 1035. | 2730. | 61 | 61 | 61 | 2730. | 61 | 1035. |
| 1072. | 1900. | 62 | 62 | 62 | 1900. | 62 | 1072. |
| 826. | 1439. | 63 | 63 | 63 | 1439. | 63 | 826. |
| 21 | 1312. | 64 | 64 | 64 | ÷ 3000. | 64 | 21 |
| 1356. ± 50 | 2800. | 65 | 65 | 65 | 2800. | 65 | 1356. ± 50 |
| 24 | 1407. | 66 | 66 | 66 | 2600. | 66 | 24 |
| 146. | 2600. | 67 | 67 | 67 | 2600. | 67 | 146. |
| 23 | 1497. | 68 | 68 | 68 | 2900. | 68 | 23 |
| 1545. | 1727. | 69 | 69 | 69 | 1727. | 69 | 1545. |
| 824. ± 5 | 1427. | 70 | 70 | 70 | 824. ± 5 | 1427. | 824. ± 5 |
| 1652. | 3327. | 71 | 71 | 71 | 3327. | 71 | 1652. |
| 2150. | 5400. | 72 | 72 | 72 | 5400. | 72 | 2150. |
| 3 | 2996. | 73 | 73 | 73 | 5425 ± 100 | 73 | 3 |
| 27 | 3410. ± 20 | 74 | 74 | 74 | 5927. | 74 | 27 |
| 7 | 3180. | 75 | 75 | 75 | 5627. | 75 | 7 |
| 4 | 3000. ± 10 | 76 | 76 | 76 | 5000. | 76 | 4 |
| 4 | 2410. | 77 | 77 | 77 | 4527 ± 100 | 77 | 4 |
| 7 | 1769. | 78 | 78 | 78 | 3827 ± 100 | 78 | 7 |
| 1 | 1063. | 79 | 79 | 79 | 2966. | 79 | 1 |

*Thermal neutron absorption cross section (2200 m⁻¹/s) barns
BNL-325, Second Edition and Supplement No. 1.

| PERIOD | Atom-ic No. Z | Sym- bol | Average thermal neutron absorption cross section barns* | Density (at 20°C except as noted) g./cc. | Modulus of elasticity (tension) $\times 10^4$ psi | Electrical resistivity microhm./cm. | Latent heat of fusion cal./g. | Specific heat cal./g./°C | Coefficient of linear thermal expansion $\times 10^{-4}/°C$ | Thermal conductivity cal./cm./°C/sec. | Melting point °C | Boiling point °C | Atom-ic No. Z |
|--------|------------------|-------------|---|---|---|-------------------------------------|-------------------------------|--------------------------|---|---------------------------------------|------------------|------------------|------------------|
| Y | 80 | Hg | 380. | 13.546 | 98.4 (50°) | 2.7 | 0.033 | 2.7 | 0.0201 | 356.58 | 80 | 356.58 | 80 |
| | 81 | Tl | 3.4 | 11.85 | 18.0 (0°) | 5.04 | 0.031 | 28. | 0.093 | 1457 ± 10 | 81 | 1457 ± 10 | 81 |
| | 82 | Pb | 0.17 | 11.35 | 2.6 | 6.3 | 0.031 | 29.3 | 0.083 | 327.5 | 82 | 1744. | 82 |
| | 83 | Bi | 0.034 | 9.747 | 4.6 | 12.5 | 0.029 | 13.3 | 0.020 | 271.3 ± 0.1 | 83 | 1560 ± 5 | 83 |
| | 84 | Po | 9.32 | 42. | | | | | | 254. | 84 | 962. | 84 |
| | 85 | At | | | | | | | | -71. | 85 | -61.8 | 85 |
| | 86 | Rn | | 0.000973 | | | | | | 700. | 86 | 700. | 86 |
| | 7 | Rf | 20. | ÷ 5. | | | | | | 1050. ± 50 | 87 | 1737. | 87 |
| | 87 | | | | | | | | | 1700. | 88 | 1737. | 88 |
| | 88 | Ra | | | | | | | | ÷ 3000. | 89 | ÷ 3000. | 89 |
| | 89 | Ac | 510. | | | | | | | ÷ 4000. | 90 | ÷ 4000. | 90 |
| | 90 | Th | 7.56 | 11.66 | 7.10. | 13.0 (0°) | 19.82 | 0.034 | 12.5 | 0.090 | | | |
| | 91 | Pa | 260. | 15.37 | | | | | | | | | |
| | 92 | U | 7.68 | 18.95 | 24.0 | 30. | 11.3 | 0.028 | 0.064 | 1132.3 ± 0.8 | 91 | 3818. | 92 |
| | 93 | Np | | 18.0 (20.45) | | | | | | 640 ± 1 | 93 | 640 ± 1 | 93 |
| | 94 | Pu | | 19.84 ²⁵ | 14.0 | 145.4 (107 [±]) | 3.3 | 0.033 | 48.4 | 630 ± 2 | 94 | 3235 ± 19 | 94 |
| | 95 | An | | 11.7 | 143. | | | | | > 800. | 95 | 2600. | 95 |
| | 96 | Cm | | ÷ 7. | | | | | | | | | |
| | 97 | Bk | | | | | | | | | | | |
| | 98 | Cf | | | | | | | | | | | |
| | 99 | Es | | | | | | | | | | | |
| | 100 | Fm | | | | | | | | | | | |

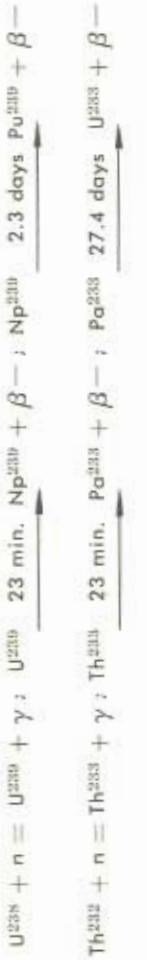
NUMEC

FISSION REACTIONS

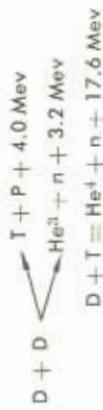
Energy released E (Mev), prompt neutrons v , ratio values of delayed to prompt neutrons β , per thermal fission

| | Total Energy of light fragments | Total Energy of heavy fragments | Total Energy of γ rays | Total Energy of fission neutron | Total Energy of beta rays | Total Energy | v | β |
|-------------------|---------------------------------|---------------------------------|-------------------------------|---------------------------------|---------------------------|--------------|------|---------|
| U ²³³ | 97 | 66 | 14 | 5 | 9 | 191 | 2.51 | 0.0026 |
| U ²³⁵ | 98 | 67 | 15 | 4.9 | 9 | 194 | 2.47 | 0.0064 |
| Pu ²³⁹ | 100 | 72 | 14 | 5.8 | 9 | 201 | 2.91 | 0.0021 |

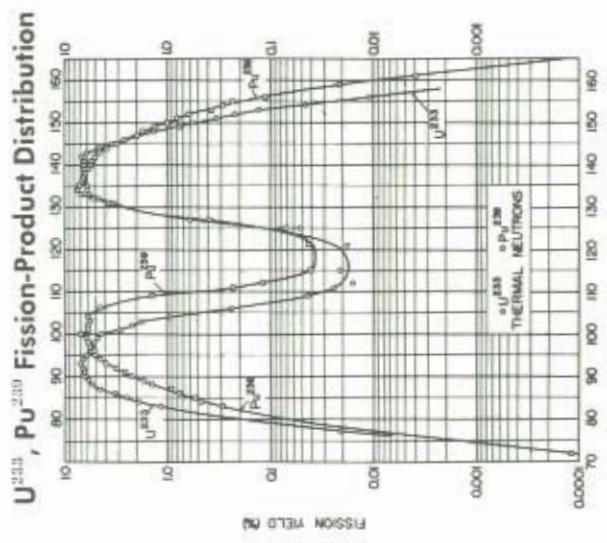
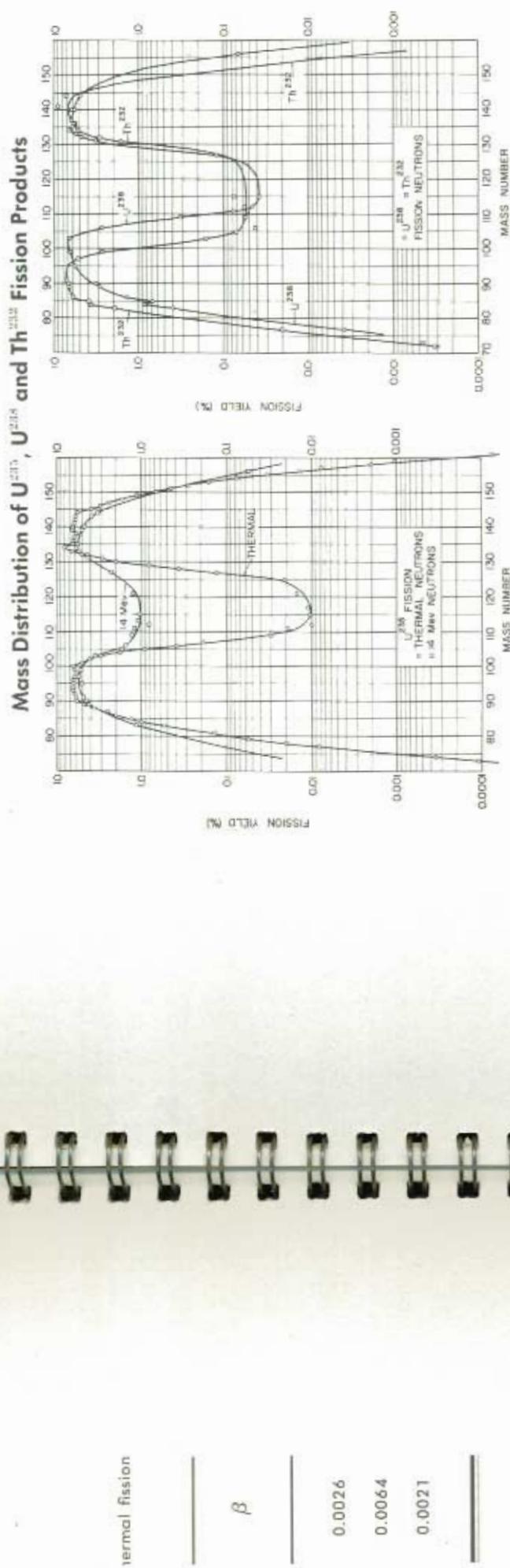
BREEDING PROCESSES



THERMONUCLEAR REACTIONS



FISSION FRAGMENTS FISSION YIELD (%) yield vs. mass number for thermal fission



From S. Katcoff, Brookhaven National Laboratory, Nucleonics—Nov. 1960

FUNDAMENTAL PHYSICAL CONSTANTS

| Symbol | Quantity | Value |
|---------------------------|---|---|
| $\alpha_0 = \eta^2/m e^2$ | First Bohr Radius | $5.291659 \pm 0.000026 \times 10^{-9} \text{ cm}$ |
| $1/\alpha = \eta c/e^2$ | Fine Structure Constant | 137.0389 ± 0.000006 |
| c | Velocity of Light | $2.997925 \pm 0.000002 \times 10^{10} \text{ cm sec}^{-1}$ |
| ϵ | Base of Natural Logarithms | 2.7182818 |
| e | Electronic Charge | $4.80296 \pm 0.00006 \times 10^{-10} \text{ esu}$ |
| e^2 | | $1.43989 \pm 0.00006 \times 10^{-7} \text{ ev cm}$ |
| e/c | | $1.602095 \pm 0.000022 \times 10^{-26} \text{ esu}$ |
| e/m | Charge to Mass Ratio of the Electron | $5.277241 \pm 0.000015 \times 10^{17} \text{ esu gm}^{-1}$ |
| e/mc | | $1.75889 \times 10^7 \text{ esu gm}^{-1}$ |
| $F = Ne/c$ | Faraday Constant (Phys. Scale) | $9648.73 \pm 0.04 \text{ esu gm}^{-1} \text{ mole}^{-1}$ |
| γ_p | Gyromagnetic Ratio of Proton, corrected for Diamagnetism | $2.675192 \pm 0.000007 \text{ radians sec}^{-1} \text{ gauss}^{-1}$ |
| h | Planck's Constant | $6.62554 \pm 0.00015 \times 10^{-27} \text{ erg sec}$ |
| $\eta = h/2\pi$ | | $1.05449 \pm 0.00003 \times 10^{-27} \text{ erg sec}$ |
| h/e | | $1.379469 \pm 0.000013 \times 10^{-17} \text{ erg sec esu}^{-1}$ |

PREFIXES FOR UNITS ADOPTED BY NBS

February 1963

The National Bureau of Standards has accepted the recommendations of the International Committee on Weights and Measures, adopting the following new prefixes for denoting multiples and sub-multiples of units:

| Order | Prefix | Symbol | Pronunciation | Order | Prefix | Symbol | Pronunciation |
|-----------|--------|--------|---------------|------------|--------|--------|---------------|
| 10^{12} | tera | T | ter'a | 10^{-2} | centi | c | sen'ti |
| 10^9 | giga | G | ji'ga | 10^{-3} | milli | m | mi'l'i |
| 10^6 | mega | M | meg'a | 10^{-6} | micro | μ | mi'kro |
| 10^3 | kilo | k | kil'o | 10^{-12} | pico | p | pe'co |
| 10^2 | hecto | h | hek'to | 10^{-15} | femto | f | fem'to |
| 10 | deka | da | deka | 10^{-18} | atto | a | at'to |
| 10^{-1} | deci | d | deci | | | | |

RADIOISOTOPE DEFINITIONS

Carrier-Free (CF) — A carrier-free radioisotope of an element is one in which all the atoms of the element that are present are atoms of this radioisotope. However, this ideal is usually only approached; carrier-free is used to mean no added carrier.

Concentration — Concentration is the solution concentration of the radioactivity and is usual expressed as millicuries per milliliter (mc/ml), millicuries per gram (mc/g), or millicuries per milligram (mc/mg).

Cross Section — The neutron activation cross section is a measure of the probability of interaction between a target nucleus and neutrons to produce a specified radioactive nuclide and is usually expressed in barns ($1 \text{ barn} = 10^{-24} \text{ cm}^2$). The values ordinarily listed in cross section tables are the isotopic cross sections; that is, they are applicable only to the particular isotope under consideration. The activation cross section used in calculating the production of a specified radioisotope from the normal element is obtained by multiplying the isotopic cross section by the isotopic abundance.

Some neutrons are absorbed to produce other radioisotopes or stable nuclides in the same element; the total absorption cross sections may be found in references such as "Neutron Cross Sections," a compilation of the Atomic Energy Commission Neutron Cross Sections Advisory Group, BNL-325 (July 1, 1958), or "Nuclear Data," a compilation of the National Bureau of Standards Nuclear Data Group, NBS Circular 499 (September 1, 1955).

Curie — A curie is that quantity of a radioisotope required to supply 3.7×10^{10} disintegrations per second (d/sec). When there is an indeterminate mixture of radioisotopes and an absolute measurement cannot be made, a curie is taken as 3.7×10^{10} beta counts/sec, estimated by standard counting procedures and corrected only for counting geometry. One one-thousandth of a curie ($3.7 \times 10^7 \text{ d/sec}$) is termed 1 millicurie (mc). One one-millionth of a curie ($3.7 \times 10^4 \text{ d/sec}$) is termed 1 microcurie (c).

Electron Capture (EC) — Electron capture is a mode of radioactive decay involving the capture of an orbital electron by its nucleus. Capture from a particular electron shell is designated as K-electron capture or L-electron capture.

Half-Life — The half-life of a radioisotope, one of the fundamental characteristics used to identify a partic-

ular radioactive species, is the time required for one-half the atoms to decay.

Isomeric Transition (IT) — Isomeric transition is the process by which a nuclide decays to an isomeric nuclide (one of the same mass number and atomic number) of lower energy. Isomeric transitions proceed by gamma ray and/or by internal conversion electron emission.

Million Electron Volts (MeV) — The energies of radiations listed herein, unless otherwise indicated, are MeV units.

Purity — Purity, as is radiochemical purity, that is, the relative freedom from other radioelements contributing contamination activities. In this respect, daughter activity and activity from radioisotopes of the same element are not considered impurities. For example, the presence of Sb²⁴ in Sb¹²² would not be considered in calculating the purity of the Sb¹²². The approximate amount of such isotopes present, however, is usually given with each shipment.

Radioactive Decay — Radioactive decay is a probability process, and the rate of decay is proportional to the number of radioactive atoms present at any time.

rhm — The abbreviation for 1 roentgen per hour at 1 meter is rhm.

Roentgen — Roentgen is defined by the Radiological Congress (Chicago, 1937) as: "The quantity of X or gamma radiation such that the associated corpuscular emission per 0.001293 g of air (= 1 cc, STP) produces, in air, ions carrying 1 electrostatic unit of quantity of electricity of either sign." A roentgen is equivalent to 1.61×10^{12} ion pairs per gram of air or the absorption of 83.8 ergs of energy per gram of air. One one-thousandth of a roentgen is termed 1 milliroentgen (mr).

Roentgen Equivalent Physical (rep) — The quantity of ionizing radiation required to produce an energy absorption of 93 ergs per gram of tissue is defined as rep.

Specific Activity — Specific activity is taken as the amount of radioactive isotope present per unit weight of total element and is usually expressed in curies or milli-curies per gram.

Standard Temperature and Pressure (STP) — STP is a temperature of 0°C and a pressure of 760 mm Hg.

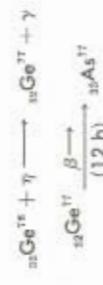
METHODS OF RADIOISOTOPE PRODUCTION

Radioisotopes are produced in a nuclear reactor by several different processes. Those processes that produce appreciable quantities of radioisotopes are described below.

1. (γ ; γ) Process.— In the (γ ; γ) process, which is most common, a neutron is captured by a target atom, and a gamma photon is emitted immediately. Since no change of the atomic number (charge on the nucleus) occurs, the element remains the same as the target material. The radioelement cannot be separated chemically unless a recoil collection is made, as in the Szillard-Chalmers process. The (γ ; γ) reaction is primarily a thermal-neutron (low-energy) reaction. For example:



A radioisotope produced by this method sometimes decays by beta emission to a radioactive daughter with a different atomic number. The daughter can be separated chemically to obtain high specific activity material. For example:



2. (γ , ρ) Process.— In the (γ , ρ) process, which requires neutrons of higher-than-thermal energies, a neutron enters a target nucleus with sufficient energy to cause a proton to be released. The atomic number is reduced by 1, and the affected atom is

transmuted into a different element, which can be separated chemically from the target material. Through the chemical separation, high-specific-activity material can be obtained. For example:



3. (γ , α) Process.— The (γ , α) process, like the (γ , ρ) process, requires high-energy neutrons. In the (γ , α) process, a neutron of very high energy enters a target atom and causes an alpha particle to be emitted. The atomic number of the target atom is reduced by 2, and a chemical separation is possible. By means of chemical separation, high-specific-activity material can be obtained. For example:



4. Fission.— In the fission process most of the fragments of uranium atoms which have undergone fission are radioactive atoms ranging from atomic number 30 through atomic number 64. They can be concentrated chemically for high specific activities, but, since several isotopes of any one element are often produced, the isotopic purity will not necessarily be as high as that of radioisotopes produced by (γ , ρ) and (γ , α) reactions. The isotopic purity will depend somewhat upon the length of time that the uranium was exposed to neutrons and upon the elapsed time between removal from the reactor and the chemical separation.

ACTIVITY PRODUCTION CALCULATION

The basic equation used in calculating activity yields is

$$A = N f \sigma S$$

where A is the activity in disintegrations per second, N is the number of atoms of the target nuclide, f is the neutron flux per square centimeter per second, σ is the activation cross section for the reaction in square centimeters per atom, and S is the saturation factor $(1 - e^{-\lambda t})$, which is the ratio of the amount of the activity produced in time t to that produced in infinite time. The decay constant, λ , is related to the half-life of the radio-nuclide produced ($\lambda = 0.693/\text{half-life}$). Hence $S = (1 - e^{-\lambda T})$, where T = half-life. The activity in disintegrations per second, A , may be converted to millicuries by dividing by 3.7×10^7 d/sec/mc.

A typical example in the application of this equation is given below for calculating the millicuries of Na^{24} activity produced in an irradiation time of seven days. The stable nuclide Na^{23} is

100% abundant; the activation cross section for the (γ , γ) reaction is 0.6 ± 0.2 barn, the half-life of Na^{24} is 15.06 hr, and the target material is 0.6 g of Na_2CO_3 (0.26 g of Na). The saturation factor, $S(1 - e^{-\lambda t})$, is 1.0 for a seven-day irradiation of a nuclide with a 15-hr half-life. The neutron flux used is 5×10^{11} neutrons/cm²/sec. The number of atoms, N , is Avogadro's number (6.02×10^{23}) times the weight of sodium [in grams] in the target divided by the gram atomic weight of the sodium atom, 23.

$$\text{Na}^{24} = \frac{(6.02 \times 10^{23})(5 \times 10^{11})(0.6 \times 10^{-3})(1)(1)(0.26)}{(23)(3.7 \times 10^7)} = 55.2 \text{ mc}$$

The specific activity of sodium is $\frac{55.2 \text{ mc}}{0.26 \text{ g}} = 212 \text{ mc per gram of sodium.}$

In cases where t is not very large compared with T , the saturation factor may be obtained by referring to page 13.

DECAY OF A RADIODELEMENT

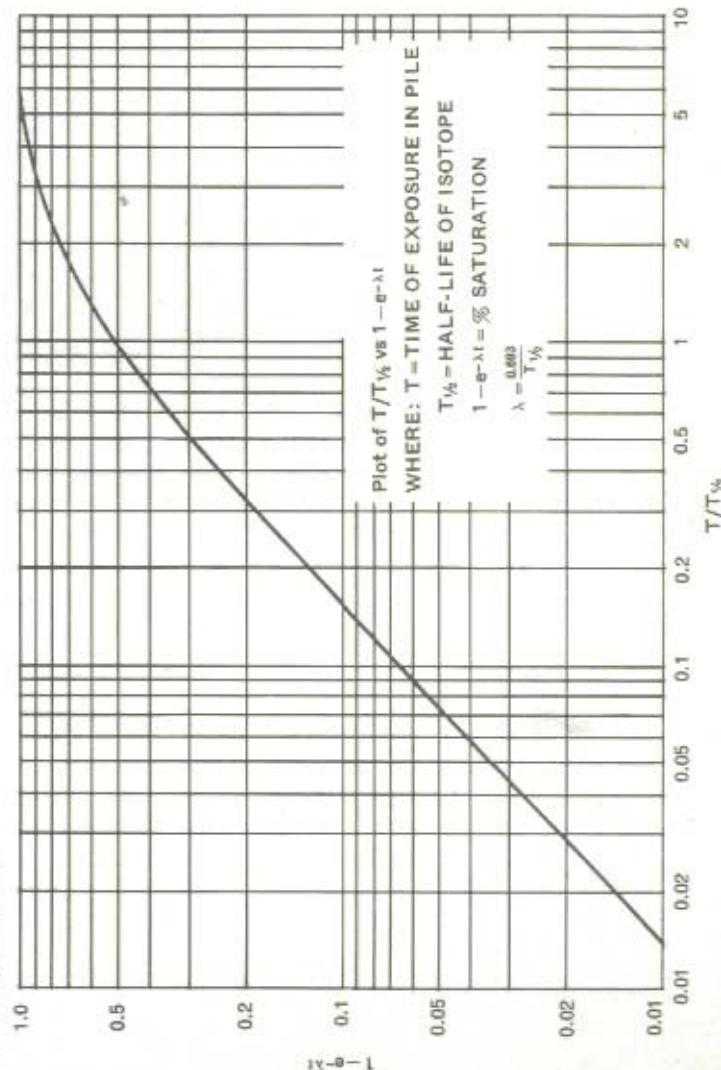
which can be separated through the chemical separation can be obtained. For

$\beta^+ + \rho$ ke the (η, ρ) process, re-a) process, a neutron of n and causes an alpha er of the target atom is an is possible. By means activity material can be

$\beta^+ \rightarrow \alpha$ set of the fragments of fission are radioactive through atomic number y for high specific activi-one element are often necessarily be as high as and (η, α) reactions. The upon the length of time ns and upon the elapsed ictor and the chemical

| Half-Lives | F* | Half-Lives | F* | Half-Lives | F* | Half-Lives | F* |
|------------|-------|------------|-------|------------|-------|------------|-------|
| 0.00 | 1.000 | 0.70 | 0.616 | 1.65 | 0.319 | 3.20 | 0.109 |
| 0.02 | 0.986 | 0.75 | 0.595 | 1.70 | 0.308 | 3.30 | 0.102 |
| 0.04 | 0.973 | 0.80 | 0.574 | 1.75 | 0.297 | 3.40 | 0.095 |
| 0.06 | 0.959 | 0.85 | 0.555 | 1.80 | 0.287 | 3.50 | 0.088 |
| 0.08 | 0.946 | 0.90 | 0.535 | 1.85 | 0.277 | 3.60 | 0.083 |
| 0.10 | 0.933 | 0.95 | 0.518 | 1.90 | 0.268 | 3.70 | 0.077 |
| 0.12 | 0.920 | 1.00 | 0.500 | 1.95 | 0.259 | 3.80 | 0.072 |
| 0.14 | 0.908 | 1.05 | 0.483 | 2.00 | 0.250 | 3.90 | 0.067 |
| 0.16 | 0.895 | 1.10 | 0.467 | 2.10 | 0.233 | 4.00 | 0.063 |
| 0.18 | 0.883 | 1.15 | 0.451 | 2.20 | 0.218 | 4.10 | 0.058 |
| 0.20 | 0.871 | 1.20 | 0.435 | 2.30 | 0.203 | 4.20 | 0.054 |
| 0.25 | 0.841 | 1.25 | 0.421 | 2.40 | 0.189 | 4.30 | 0.051 |
| 0.30 | 0.812 | 1.30 | 0.406 | 2.50 | 0.177 | 4.40 | 0.047 |
| 0.35 | 0.785 | 1.35 | 0.393 | 2.60 | 0.165 | 4.50 | 0.044 |
| 0.40 | 0.758 | 1.40 | 0.379 | 2.70 | 0.154 | 4.60 | 0.041 |
| 0.45 | 0.732 | 1.45 | 0.367 | 2.80 | 0.144 | 4.70 | 0.039 |
| 0.50 | 0.707 | 1.50 | 0.354 | 2.90 | 0.134 | 4.80 | 0.036 |
| 0.55 | 0.683 | 1.55 | 0.342 | 3.00 | 0.125 | 4.90 | 0.034 |
| 0.60 | 0.660 | 1.60 | 0.330 | 3.10 | 0.117 | 5.00 | 0.031 |
| 0.65 | 0.638 | | | | | | |

* F = fraction remaining.



tion for the (η, γ) reaction 15.06 hr, and the target a). The saturation factor, lation of a nuclide with is 5×10^{11} neutrons/cm²/ ro's number (6.02×10^{23}) in the target divided by atom, 23.

$1/(1 - e^{-\lambda t}) = 55.2$ mc

pared with T, the saturation to page 13.

EXEMPT QUANTITIES OF RADIOISOTOPES

Exempt quantities of radioisotopes are available under general license and do not require a specific AEC license for procurement and possession. Exempt quantities are shown in Title 10, Part 31 of the Federal Register.

| Exempt Quantities of Byproduct material | Column No. I Not as a sealed source [micro-curies] | | Column No. II As a sealed source [micro-curries] | | Exempt Quantities of Byproduct material [micro-curies] | Column No. I Not as a sealed source [micro-curries] | |
|---|---|---|---|---|--|--|---|
| | Column No. I Not as a sealed source [micro-curies] | Column No. II As a sealed source [micro-curries] | Column No. I Not as a sealed source [micro-curries] | Column No. II As a sealed source [micro-curries] | | Column No. I Not as a sealed source [micro-curries] | Column No. II As a sealed source [micro-curries] |
| Antimony (Sb 124) | 1 | 10 | Palladium 103—Rhodium 103 | 50 | 50 | 10 | 10 |
| Arsenic 76 (As 76) | 10 | 10 | (Pd-Rh 103) | 10 | 10 | 10 | 10 |
| Arsenic 77 (As 77) | 10 | 10 | Phosphorus 32 (P 32) | 0.1 | 1 | 10 | 10 |
| Barium 140—Lanthanum 140 (Ba-La 140) | 1 | 10 | Polonium 210 (Po 210) | 10 | 10 | 10 | 10 |
| Beryllium (Be 7) | 50 | 50 | Potassium 42 (K 42) | 10 | 10 | 10 | 10 |
| Cadmium 109—Silver 109 (Cd-Ag 109) | 10 | 10 | Praseodymium 143 (Pr 143) | 10 | 10 | 10 | 10 |
| Calcium 45 (Ca 45) | 10 | 10 | Promethium 147 (Pm 147) | 10 | 10 | 10 | 10 |
| Carbon 14 (C 14) | 50 | 50 | Rhenium 186 (Re 186) | 10 | 10 | 10 | 10 |
| Cerium 144—Praseodymium (Ce-Pr 114) | 1 | 10 | Rhodium 105 (Rh 105) | 10 | 10 | 10 | 10 |
| Cesium—Barium 137 (Ce-Ba 137) | 1 | 10 | Rubidium 86 (Rb 86) | 10 | 10 | 10 | 10 |
| Chlorine 36 (Cl 36) | 1 | 10 | Ruthenium 106—Rhodium 106 (Ru-Rh 106) | 10 | 10 | 10 | 10 |
| Chromium 51 (Cr 51) | 50 | 50 | Samarium 153 (Sm 153) | 10 | 10 | 10 | 10 |
| Cobalt 60 (Co 60) | 1 | 10 | Scandium 46 (Sc 46) | 1 | 10 | 10 | 10 |
| Copper 64 (Cu 64) | 50 | 50 | Silver 105 (Ag 105) | 10 | 10 | 10 | 10 |
| Europium 154 (Eu 154) | 1 | 10 | Silver 111 (Ag 111) | 10 | 10 | 10 | 10 |
| Fluorine 18 | 50 | 50 | Sodium 22 (Na 22) | 10 | 10 | 10 | 10 |
| Gallium 72 (Ga 72) | 10 | 10 | Sodium 24 (Na 24) | 10 | 10 | 10 | 10 |
| Germanium 71 (Ge 71) | 50 | 50 | Strontrium 89 (Sr 89) | 1 | 10 | 10 | 10 |
| Gold 198 (Au 198) | 10 | 10 | Strontium 90—Yttrium 90 (Sr-Y-90) | 0.1 | 1 | 10 | 10 |
| Gold 199 (Au 199) | 10 | 10 | Sulfur 35 (S 35) | 50 | 50 | 10 | 10 |
| Hydrogen 3 (Tritium) (H 3) | 250 | 250 | Tantalum 182 (Ta 182) | 10 | 10 | 10 | 10 |
| Indium 114 (In 114) | 1 | 10 | Technetium 96 (Tc 96) | 1 | 10 | 10 | 10 |
| Iodine 131 (I 131) | 10 | 10 | Technetium 99 (Tc 99) | 1 | 10 | 10 | 10 |
| Iridium 192 (Ir 192) | 10 | 10 | Tellurium 127 (Te 127) | 10 | 10 | 10 | 10 |
| Iron 55 (Fe 55) | 50 | 50 | Tellurium 129 (Te 129) | 1 | 10 | 10 | 10 |
| Iron 59 (Fe 59) | 1 | 10 | Thallium 204 (Tl 204) | 50 | 50 | 10 | 10 |
| Lanthanum 140 (La 140) | 10 | 10 | Tin 113 (Sn 113) | 10 | 10 | 10 | 10 |
| Manganese 52 (Mn 52) | 1 | 10 | Tungsten 185 (W 185) | 10 | 10 | 10 | 10 |
| Manganese 56 (Mn 56) | 50 | 50 | Vanadium 48 (V 48) | 1 | 10 | 10 | 10 |
| Molybdenum 99 (Mo 99) | 10 | 10 | Yttrium 90 (Y 90) | 1 | 10 | 10 | 10 |
| Nickel 59 (Ni 59) | 1 | 10 | Yttrium 91 (Y 91) | 1 | 10 | 10 | 10 |
| Nickel 63 (Ni 63) | 1 | 10 | Zinc 65 (Zn 65) | 10 | 10 | 10 | 10 |
| Niobium 95 (Nb 95) | 10 | 10 | Beta and/or gamma emitting by-product material not listed above | 1 | 10 | 10 | 10 |
| Palladium 109 (Pd 109) | 10 | 10 | product material not listed above | 1 | 10 | 10 | 10 |

RADIOISOTOPES FOR HEAT SOURCES

| Isotope in order of decreasing half-life | Compound | Warts per gram | Density of semi- precious stone per cm. ³ | Power density of thermal watts per cm. ³ | Half-life years at 600 cm. cm | Cast & thermal heat | Curing power thermal heat | Power after 5 years initial power | Shielding thickness of uranium per 100 watt source |
|---|--------------------------------|--------------------|--|---|--|---------------------------|------------------------------------|---|--|
| Americium, 34 Am | Methyl | 0 | .1 | 1.7 | 1.17 | Minor | 4.68, | \$1,820 | .30 |
| Plutonium, 238 Pu | PuO ₂ | 0 | .39 | 10.0 | 3.9(a) | Minor | .894 | .985 | .961 |
| Uranium, 232 U | UO ₂ | $\alpha\gamma$ | 1.3 | 10.0 | 33.0 | Heavy | .74, | .350 | .981 |
| Uranium, 137 Cs | Borosilicate | $\beta\gamma$ | .0774 | 3.1 | .24 | 8.4 | 30±.3 | 109(216) | 207 |
| SrO | $\beta\gamma$ | .334 | 4.5 | 1.5 | 4.4 | 27.7 | 111(196) | 150 | .951 |
| SrO | $\beta\gamma$ | .223 | 3.7 | .825 | 4.4 | 27.7 | 111(196) | 150 | .951 |
| SrTiO ₃ | $\alpha\gamma\eta$ | 2.5 | 9.0 | 22.5 | Neutron Shield | 18.4 | 3.57 | .30 | .927 |
| Zirconium, 244 Cm | Cm ₂ O ₃ | $\beta\gamma$ | 5.52 | 8.7 | .48 | 9.5 | 5.24 | .33 | .65 |
| Zoball, 60 Co | Metal | $\beta\gamma$ | .12 | 9.0 | 1.08 | Minor | .4, | 100 | .640 |
| Thallium, 204 Tl | Tl ₂ O ₃ | β | .324 | 6.6 | 2.03 | Low | 2.6 | 4,260(916) | 2,770 |
| Tronethium, 147 Pm | Pm ₂ O ₃ | β | .348 | 7.0 | 1.270 | Heavy | 1.9 | .40 | .707 |
| Thorium, 232 Th | ThO ₂ | $\alpha\gamma$ | 1.41 | 9. | 21.9 | — | .78 | 1351.000(a) | .124 |
| Cerium, 144 Ce | CeO ₃ | $\beta\gamma$ | 3.48 | 4.4, 1 | 9. | 397 | Neutron Shield | .445 | .17 |
| Cerium, 240 Ce | Ce ₂ O ₃ | $\alpha\gamma\eta$ | 4.4, 1 | — | — | — | — | — | .28 |
| Lutetium, 176 Lu | Metal | α | 134, | 9.3 | 1,210 | Minor | .38 | .20 | .32 |
| Polonium, 310 Po | ImpD ₂ | β | 1.03 | 7.7 | 7.9 | Minor | .35 | .10 | .019 |
| Hallium, 120 Tm | ImpD ₂ | β | — | — | — | — | — | — | .0005 |

1. Oak Ridge National Laboratory Report and Sample Notes (O-104). April 1943.
 2. The Fusion Products, by L. A. Sidemore, Nuclear Laboratories, May 1948.
 3. Isotope Power Data Sheets compiled by S. J. Rainbow, Oak Ridge, Tennessee.

THORIUM MATERIALS CONVERSION TABLE

| | Mol. Wt.* | Th | ThO ₂ | (TNT) | ThC | ThC ₂ | ThCl ₄ |
|---|--------------|-------|------------------|-------|-------|------------------|-------------------|
| Th Metal | 232.00 | 1.000 | 0.879 | 0.420 | 0.951 | 0.906 | 0.621 |
| ThO ₂ (Thorium Dioxide) [Thorium Nitrate Tetrahydrate (TNT)] | 264.00 | 1.138 | 1.000 | 0.478 | 1.082 | 1.031 | 0.706 |
| Th(Na ₂) ₄ · 4H ₂ O [Thorium Nitrate Tetrahydrate (TNT)] | 552.08 | 2.380 | 2.091 | 1.000 | 2.263 | 2.156 | 1.477 |
| ThC (Thorium Carbide) | 244.01 | 1.052 | 0.924 | 0.442 | 1.000 | 0.953 | 0.653 |
| ThC ₂ (Thorium Dicarbide) | 256.02 | 1.104 | 0.970 | 0.464 | 1.049 | 1.000 | 0.685 |
| ThCl ₄ (Thorium Tetrachloride) | 373.81 | 1.611 | 1.416 | 0.677 | 1.532 | 1.460 | 1.000 |

Example: 100# of ThO₂ × 0.879 = 87.9# of Th Metal obtained from ThO₂.
 *Based on C₁₂ = 12.

THORIUM DIOXIDE (ThO₂)—PERCENT THEORETICAL DENSITY (% T.D.) AND EQUIVALENT GRAMS PER CUBIC CENTIMETER (g/cc).*

| % T.D. | g/cc |
|--------|-------|--------|-------|--------|-------|--------|-------|--------|-------|--------|-------|
| 83.0 | 8.333 | 85.0 | 8.534 | 87.0 | 8.735 | 89.0 | 8.936 | 91.0 | 9.136 | 93.0 | 9.337 |
| 2 | 8.353 | 2 | 8.554 | 2 | 8.755 | 2 | 8.956 | 2 | 9.156 | 2 | 9.357 |
| 4 | 8.373 | 4 | 8.574 | 4 | 8.775 | 4 | 8.976 | 4 | 9.177 | 4 | 9.377 |
| 6 | 8.393 | 6 | 8.594 | 6 | 8.795 | 6 | 8.996 | 6 | 9.197 | 6 | 9.397 |
| 8 | 8.414 | 8 | 8.614 | 8 | 8.815 | 8 | 9.016 | 8 | 9.217 | 8 | 9.418 |
| 84.0 | 8.434 | 86.0 | 8.634 | 88.0 | 8.835 | 90.0 | 9.036 | 92.0 | 9.237 | 94.0 | 9.438 |
| 2 | 8.454 | 2 | 8.654 | 2 | 8.855 | 2 | 9.056 | 2 | 9.257 | 2 | 9.458 |
| 4 | 8.474 | 4 | 8.675 | 4 | 8.875 | 4 | 9.076 | 4 | 9.277 | 4 | 9.478 |
| 6 | 8.494 | 6 | 8.695 | 6 | 8.895 | 6 | 9.096 | 6 | 9.297 | 6 | 9.498 |
| 8 | 8.514 | 8 | 8.715 | 8 | 8.916 | 8 | 9.116 | 8 | 9.317 | 8 | 9.518 |

*Based on TD = 10.04 g/cc.

PLUTONIUM MATERIALS CONVERSION TABLE (Pu Composition 93% Pu²³⁹, 7% Pu²⁴⁰)

| ThC | ThC ₂ | ThCl ₄ | Pu Metal | Mol. Wt.* | Pu | PuO ₂ | PuCl ₃ | PuF ₃ | PuF ₄ | PuC | PuN | Pu(SO ₄) ₂ | (PuSH) |
|-------|------------------|-------------------|--|-----------|-------|------------------|-------------------|------------------|------------------|-------|-------|-----------------------------------|--------|
| 0.951 | 0.906 | 0.621 | PuO ₂ (Plutonium Dioxide) | 239.13 | 1.000 | 0.882 | 0.692 | 0.808 | 0.759 | 0.952 | 0.945 | 0.555 | 0.475 |
| 1.082 | 1.031 | 0.706 | PuCl ₃ (Plutonium Trichloride) | 271.13 | 1.134 | 1.000 | 0.785 | 0.916 | 0.860 | 1.080 | 1.071 | 0.629 | 0.539 |
| 2.263 | 2.156 | 1.477 | PuF ₃ (Plutonium Trifluoride) | 345.49 | 1.445 | 1.274 | 1.000 | 1.167 | 1.096 | 1.376 | 1.365 | 0.801 | 0.687 |
| 1.000 | 0.953 | 0.653 | PuF ₄ (Plutonium Tetrafluoride) | 296.12 | 1.238 | 1.092 | 0.857 | 1.000 | 0.940 | 1.179 | 1.170 | 0.687 | 0.588 |
| 1.049 | 1.000 | 0.685 | PuC (Plutonium Carbide) | 315.12 | 1.318 | 1.162 | 0.912 | 1.064 | 1.000 | 1.235 | 1.245 | 0.731 | 0.626 |
| 1.532 | 1.460 | 1.000 | PuN (Plutonium Nitride) | 251.14 | 1.050 | 0.926 | 0.727 | 0.848 | 0.797 | 1.000 | 0.992 | 0.582 | 0.499 |
| | | | Pu(SO ₄) ₂ (Plutonium Sulfate) | 253.14 | 1.059 | 0.934 | 0.733 | 0.855 | 0.803 | 1.008 | 1.000 | 0.587 | 0.503 |
| | | | Pu(SO ₄) ₂ · 4H ₂ O [Plutonium Sulfate Tetrahydrate (PuSH)] | 431.21 | 1.803 | 1.590 | 1.248 | 1.456 | 1.368 | 1.717 | 1.703 | 1.000 | 0.857 |
| | | | | 503.25 | 2.105 | 1.856 | 1.457 | 1.699 | 1.597 | 2.004 | 1.988 | 1.167 | 1.000 |

Example: 100# of PuCl₃ × 0.692 = 69.2# of Pu metal obtained from PuCl₃.

*Based on Cl:2 = 12.

PLUTONIUM DIOXIDE (PuO₂)—PERCENT THEORETICAL DENSITY (% T.D.) AND EQUIVALENT GRAMS PER CUBIC CENTIMETER (g/cc).*

| % T.D. | g/cc | % T.D. | g/cc | % T.D. | g/cc | % T.D. | g/cc | % T.D. | g/cc | % T.D. | g/cc | % T.D. | g/cc |
|--------|-------|--------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 83.0 | 9.516 | 85.0 | 9.745 | 87.0 | 9.975 | 89.0 | 10.204 | 91.0 | 10.433 | 93.0 | 10.662 | 95.0 | 10.892 |
| 84.0 | 9.631 | 86.0 | 9.860 | 88.0 | 10.089 | 90.0 | 10.319 | 92.0 | 10.548 | 94.0 | 10.777 | 96.0 | 11.006 |
| 85.0 | 9.558 | 82 | 9.759 | 82 | 9.768 | 82 | 10.227 | 82 | 10.456 | 82 | 10.685 | 82 | 11.121 |
| 86.0 | 9.578 | 4 | 9.779 | 82 | 9.997 | 2 | 10.227 | 2 | 10.456 | 2 | 10.915 | 2 | 11.144 |
| 87.0 | 9.598 | 6 | 9.799 | 4 | 9.791 | 4 | 10.020 | 4 | 10.479 | 4 | 10.708 | 4 | 11.167 |
| 88.0 | 9.618 | 8 | 9.819 | 6 | 9.814 | 6 | 10.043 | 6 | 10.273 | 6 | 10.502 | 6 | 11.190 |
| 89.0 | 9.638 | 8 | 9.839 | 8 | 9.837 | 8 | 10.066 | 8 | 10.296 | 8 | 10.525 | 8 | 11.213 |
| 90.0 | 9.658 | 2 | 9.859 | 2 | 9.883 | 2 | 10.112 | 2 | 10.341 | 2 | 10.571 | 2 | 11.259 |
| 91.0 | 9.678 | 4 | 9.879 | 4 | 9.906 | 4 | 10.135 | 4 | 10.364 | 4 | 10.594 | 4 | 11.282 |
| 92.0 | 9.699 | 6 | 9.899 | 6 | 9.929 | 6 | 10.158 | 6 | 10.387 | 6 | 10.617 | 6 | 11.304 |
| 93.0 | 9.719 | 8 | 9.919 | 8 | 9.952 | 8 | 10.181 | 8 | 10.410 | 8 | 10.640 | 8 | 11.327 |

*Based on TD = 11.465 g/cc.

URANIUM MATERIALS CONVERSION TABLE

| | Mol. [*] Wt. | U | UO ₂ | UO ₃ | U ₃ O ₈ | UF ₄ | UF ₆ | (UNH) | UC | UC ₂ | UN | (USH) |
|---|--------------------------|-------|-----------------|-----------------|-------------------------------|-----------------|-----------------|-------|-------|-----------------|-------|-------|
| U Metal | 238.03 | 1.000 | 0.881 | 0.832 | 0.848 | 0.758 | 0.676 | 0.474 | 0.952 | 0.908 | 0.944 | 0.567 |
| UO ₂ (Brown Oxide) | 270.03 | 1.134 | 1.000 | 0.944 | 0.962 | 0.860 | 0.767 | 0.538 | 1.080 | 1.030 | 1.071 | 0.643 |
| UO ₃ (Orange Oxide) | 286.03 | 1.202 | 1.059 | 1.000 | 1.019 | 0.911 | 0.813 | 0.570 | 1.144 | 1.091 | 1.135 | 0.681 |
| U ₃ O ₈ (Black Oxide) | 842.09 | 1.179 | 1.040 | 0.981 | 1.000 | 0.894 | 0.797 | 0.559 | 1.123 | 1.071 | 1.114 | 0.668 |
| UF ₄ (Green Salt) | 314.02 | 1.319 | 1.163 | 1.098 | 1.119 | 1.000 | 0.892 | 0.625 | 1.256 | 1.198 | 1.246 | 0.747 |
| UF ₆ (U Hexafluoride) | 352.02 | 1.479 | 1.304 | 1.231 | 1.254 | 1.121 | 1.000 | 0.701 | 1.408 | 1.343 | 1.397 | 0.838 |
| UO ₂ (NO ₃) ₂ · 6H ₂ O (Uranyl Nitrate (UNH)) | 502.13 | 2.110 | 1.860 | 1.756 | 1.789 | 1.599 | 1.426 | 1.000 | 2.008 | 1.916 | 1.992 | 1.195 |
| UC (U Monocarbide) | 250.04 | 1.050 | 0.926 | 0.874 | 0.891 | 0.796 | 0.710 | 0.498 | 1.000 | 0.954 | 0.992 | 0.595 |
| UC ₂ (U Dicarbide) | 262.05 | 1.101 | 0.970 | 0.916 | 0.934 | 0.834 | 0.744 | 0.522 | 1.048 | 1.000 | 1.040 | 0.624 |
| UN (U Nitride) | 252.04 | 1.059 | 0.933 | 0.881 | 0.898 | 0.803 | 0.716 | 0.502 | 1.008 | 0.962 | 1.000 | 0.600 |
| UO ₂ SO ₄ · 3H ₂ O (Uranyl Sulfate (USH)) | 420.14 | 1.765 | 1.556 | 1.469 | 1.497 | 1.338 | 1.194 | 0.837 | 1.680 | 1.603 | 1.667 | 1.000 |

*Based on C¹² = 12

**URANIUM DIOXIDE (UO₂)—PERCENT THEORETICAL DENSITY (% T.D.)
AND EQUIVALENT GRAMS PER CUBIC CENTIMETER (g/cc).***

(Normal Enrichment)

| % T.D. | g/cc |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 91.0 | 9.974 | 92.0 | 10.083 | 93.0 | 10.193 | 94.0 | 10.302 | 95.0 | 10.412 | 96.0 | 10.522 | 97.0 | 10.631 |
| 1 | 98.5 | 1 | 0.94 | 1 | 204 | 1 | 313 | 1 | 423 | 1 | 533 | 1 | 642 |
| 2 | 99.6 | 2 | 105 | 2 | 215 | 2 | 324 | 2 | 434 | 2 | 544 | 2 | 653 |
| 3 | 10.006 | 3 | 116 | 3 | 226 | 3 | 335 | 3 | 445 | 3 | 554 | 3 | 664 |
| 4 | 017 | 4 | 127 | 4 | 237 | 4 | 346 | 4 | 456 | 4 | 565 | 4 | 675 |
| 5 | 028 | 5 | 138 | 5 | 248 | 5 | 357 | 5 | 467 | 5 | 576 | 5 | 686 |
| 6 | 039 | 6 | 149 | 6 | 259 | 6 | 368 | 6 | 478 | 6 | 587 | 6 | 697 |
| 7 | 050 | 7 | 160 | 7 | 270 | 7 | 379 | 7 | 489 | 7 | 598 | 7 | 708 |
| 8 | 061 | 8 | 171 | 8 | 280 | 8 | 390 | 8 | 500 | 8 | 609 | 8 | 719 |
| 9 | 072 | 9 | 182 | 9 | 291 | 9 | 401 | 9 | 511 | 9 | 620 | 9 | 730 |

*Based on TD = 10.960 g/cc

BASE CHARGES FOR ENRICHED URANIUM AS UF₆

Uranium enriched in U-235 is distributed to licensees in the form of UF₆. It is shipped as a solid under pressure in steel cylinders. It is available in all enrichments from normal (0.711 weight per cent U-235) to approximately 95 weight per cent U-235.

The base charges for enriched uranium as UF₆ are as follows:

| UC | UC ₂ | UN | (USH) | Assay (weight fraction U-235) | Base charge (\$ per Kg U) | Assay (weight fraction U-235) | Base charge (\$ per Kg U) |
|-------|-----------------|-------|-------|-------------------------------|---------------------------|-------------------------------|---------------------------|
| 0.952 | 0.908 | 0.944 | 0.567 | 0.0075 | \$ 26.50 | 0.050 | \$ 479.40 |
| 1.080 | 1.030 | 1.071 | 0.643 | 0.0080 | 30.50 | 0.055 | 536.80 |
| 1.144 | 1.091 | 1.135 | 0.681 | 0.0085 | 34.70 | 0.060 | 594.50 |
| 1.123 | 1.071 | 1.114 | 0.668 | 0.0090 | 38.90 | 0.07 | 710.50 |
| 1.256 | 1.198 | 1.246 | 0.747 | 0.0095 | 43.30 | 0.08 | 827.00 |
| 1.408 | 1.343 | 1.397 | 0.838 | 0.0100 | 47.70 | 0.09 | 944.00 |
| 2.008 | 1.916 | 1.992 | 1.195 | 0.0111 | 56.80 | 0.10 | 1,062.00 |
| 1.000 | 0.954 | 0.992 | 0.595 | 0.0112 | 66.10 | 0.12 | 1,298.00 |
| 1.048 | 1.000 | 1.040 | 0.624 | 0.0113 | 75.70 | 0.14 | 1,535.50 |
| 1.008 | 0.962 | 1.000 | 0.600 | 0.0114 | 85.40 | 0.16 | 1,774.00 |
| 1.680 | 1.603 | 1.667 | 1.000 | 0.0115 | 95.30 | 0.18 | 2,013.00 |
| | | | | 0.0116 | 105.30 | 0.20 | 2,252.00 |
| | | | | 0.0117 | 115.50 | 0.25 | 2,853.00 |
| | | | | 0.0118 | 125.70 | 0.30 | 3,456.00 |
| | | | | 0.0119 | 136.10 | 0.35 | 4,060.00 |
| | | | | 0.020 | 146.50 | 0.40 | 4,666.00 |
| | | | | 0.022 | 167.60 | 0.50 | 5,882.00 |
| | | | | 0.024 | 189.00 | 0.60 | 7,103.00 |
| | | | | 0.026 | 210.60 | 0.70 | 8,329.00 |
| | | | | 0.028 | 232.40 | 0.80 | 9,562.00 |
| | | | | 0.030 | 254.30 | 0.85 | 10,183.00 |
| | | | | 0.032 | 276.40 | 0.90 | 10,808.00 |
| | | | | 0.034 | 298.60 | 0.92 | 11,061.00 |
| | | | | 0.036 | 320.90 | 0.93 | 11,188.00 |
| | | | | 0.038 | 343.30 | 0.94 | 11,315.00 |
| | | | | 0.040 | 365.80 | 0.96 | 11,597.00 |
| | | | | 0.045 | 422.40 | 0.98 | 12,389.00 |

Base charges for enriched uranium of assays not specifically listed will be determined by linear interpolation between the nearest listed assays. When the assay of enriched material is less than 0.0075 the base charge will be determined by linear interpolation between the base charge for 0.0075 material and a value of \$23.50 per Kg of normal uranium (0.00711 weight fraction U-235) in the form of UF₆.

BASE CHARGES FOR DEPLETED URANIUM AS UF₆

For depleted uranium as UF₆, without specified assay, the base charge is \$2.50 per Kg of contained U. For specifically requested assays the base charges are as follows:

| Assay (weight fraction U-235) | Base charge (\$ per Kg U) |
|----------------------------------|------------------------------|
| 0.0002 | \$3.00 |
| 0.0038 | 3.00 |
| 0.0040 | 3.70 |
| 0.0042 | 4.60 |
| 0.0044 | 5.60 |
| 0.0046 | 6.65 |
| 0.0048 | 7.75 |
| 0.0050 | 8.90 |
| 0.0052 | 10.10 |
| 0.0054 | 11.35 |
| 0.0056 | 12.65 |
| 0.0058 | 13.95 |
| 0.0060 | 15.35 |
| 0.0065 | 18.90 |
| 0.0070 | 22.60 |

Base charges for depleted uranium of assays not specifically listed will be determined by linear interpolation between the nearest listed assays. When the assay of depleted materials is greater than 0.0070, the base charge will be determined by linear interpolation between the base charge for 0.0070 material and a value of \$23.50 per Kg U for normal uranium (0.0071) weight fraction U-235) in the form of UF₆.

USE CHARGES FOR SPECIAL NUCLEAR MATERIAL

Title to all special nuclear material remains with the United States Government. Special nuclear material is leased to licensees on an annual use charge of 4% percent of its value as determined from the appropriate schedule of charges.

The use charge, based on the UF₆ value of the material, commences on the date the material is diverted from Commission production channels; it continues either until (1) the material, or part of it, is returned to the Commission, at which time the licensee is credited for the value of the material returned, less any charges for processing to specification, and makes settlement; or until (2) the licensee declares that all or some part of the material has been burned, lost, or otherwise consumed — and the licensee makes payment. Oak Ridge, Tenn., is the FOB point for distribution and return of UF₆.

AEC CHARGES FOR CONVERSION OF U_3O_8 TO UF_6

Recovered uranium bearing materials are usually returned to the AEC in the form of U_3O_8 for conversion to UF_6 . AEC charges for this service are as follows:

| | |
|--------------------------------------|----------------------------|
| Materials of up to 5% enrichment | \$ 5.60 per Kg contained U |
| Materials of more than 5% enrichment | \$32.00 per Kg contained U |

In addition, cost allowance should also be made for processing losses of 1.6 grams per Kg of U returned as well as 20 days use charges per Kg of U returned.

NOTE: Reference, USAEC-TID-4020, Revision 1, September 1961

AEC WITHDRAWAL AND CERTIFICATION CHARGES FOR UF_6

Charges for withdrawing and packaging UF_6 into individual containers are given in Column 1. If a single order is packaged into more than one container of the same type, the samples which are taken for determination of the properties may sometimes be composited into a single analytical lot. If this is done, the charges given in Column III are appropriate for all cylinders from which samples are so composited, excepting the first one of each lot. The maximum number of cylinders from which samples may be composited is given in Column III. Unless specifically requested otherwise, the AEC will composite to the maximum extent possible.

WITHDRAWAL AND PACKAGING CHARGES

| Cylinder type | Column I, single cylinder or first cylinder in composite, analytical lot (\$ per cylinder) | Column II, remaining cylinders in composite, analytical lot (\$ per cylinder) | Column III, maximum number of cylinders per com- posite, analytical lot (\$ per cylinder) |
|---------------|--|--|---|
| 10-ton | 8.50 | Not composited | |
| 2.5-ton | 3.75 | 23.5 | 3 |
| 1/2-inch (MD) | 1.50 | 7.0 | 6 |
| 8-inch | 1.43 | 6.3 | 6 |
| 5-inch | 1.35 | 5.5 | 6 |
| 4-inch | 1.15 | Not composited | |
| Harshaw bomb | 5.8 | Not composited | |
| 2-inch | 5.8 | Not composited | |
| Hole tube | 2.9 | Not composited | |

(1) 8-inch cylinders are used only for assays of 0.0275 to 0.125 weight fraction $\text{U}-235$ inclusive.

SPECIAL CERTIFICATION CHARGES

| Property or condition to be certified | Charge (per cylinder) |
|---|--------------------------|
| A. Total Pressure | \$ 7 |
| B. Spectrographic Impurities | 158 |
| C. Bromine and Chlorine | 36 |
| D. Freezing-point Depression | 1.4 |
| E. Non-volatile Matter | 36 |
| F. Baro-equivalent Cross Section | 36 |
| G. Molybdenum, Vanadium, Chromium, and Tungsten (Molybdenum only, \$29) | 65 |
| H. Fission-product and U-237 Gamma Activity | 28 |
| I. Fission-product Beta Activity | 22 |
| J. Plutonium Content | 22 |
| Total | \$424 |

Kg of con-

nuclear ma-
terial is di-
part of it, is
material re-
sponsible
for the license
and
rn of UF_6 .

LOADING LIMITS ON AEC UF₆ CYLINDERS⁽¹⁾

| Assay (weight fraction U-235) | Maximum quantity per cylinder, pound UF ₆ | | | | |
|-------------------------------|--|---------|--------------|----------|--------|
| | 10-ton | 2.5-ton | 12-inch (MD) | 8-inch | 5-inch |
| 0.0095 or less | 21,000 | 4,800 | 450 | Not used | 55 |
| Above 0.0095 to 0.0100 | 0 | 4,800 | 450 | Not used | 55 |
| Above 0.0100 to 0.0110 | 0 | 4,417 | 450 | Not used | 55 |
| Above 0.0110 to 0.0120 | 0 | 2,445 | 450 | Not used | 55 |
| Above 0.0120 to 0.0125 | 0 | 1,800 | 450 | Not used | 55 |
| Above 0.0125 to 0.0375 | 0 | 0 | 450 | Not used | 55 |
| Above 0.0375 to 0.125 | 0 | 0 | 0 | 250 | 55 |
| Above 0.125 | 0 | 0 | 0 | 0 | 55 |

(1) Cylinders loaded to these limits may require special precautions in storage and shipment to avoid the possibility of nuclear interaction with adjacent cylinders or with moderators and reflectors other than water. The loading limit on a 4-inch cylinder is 11 pounds, on a bomb is 4.8 pounds, on a 2-inch cylinder is 3.3 pounds and on a Hooke tube is 1.5 grams at all enrichments.

AEC CHARGES FOR CONTAINED PLUTONIUM ISOTOPES

Pu-239 plus Pu-241

The AEC has established base charges for material of standard isotopic assays. Charges for plutonium nitrate distributed by lease after July 1, 1963 are \$43 per gram of the contained plutonium isotopes Pu-239 plus Pu-241.

Reduced base charges are applicable in cases in which the AEC has determined that the use of such material will produce technical and economic data of sufficient interest in the AEC program and the lessee has agreed to extend to the AEC access to such data and appropriate patent rights. Under these conditions, plutonium nitrate charges are \$10 per gram of the contained plutonium isotopes Pu-239 plus Pu-241.

The total charge for conversion of plutonium nitrate to metal is \$1.50 per gram of plutonium metal distributed, plus use charges and a charge for loss of an amount of plutonium during conversion equal to 1.0 percent of plutonium metal distributed multiplied by the base charges set forth above. A special charge is also made by the AEC for packaging plutonium into suitable containers; these charges are not refunded upon return of leased material.

AEC CHARGES FOR URANIUM ENRICHED IN U-233

Effective July 1, 1963, the AEC established base charges for material of standard isotopic assays. Charges for uranyl nitrate containing uranium enriched in U-233 are \$82 per gram of contained U-233. Base charges, however, are subject to adjustments for the isotopic assay which follows.

- (1) Calculate a weight fraction equal to the ratio of the weight of U-235 plus U-233 to the total weight of uranium. For that weight fraction, find the charge per gram of U-235 from the schedule of base charges in effect for uranium enriched in U-235. (If the weight fraction exceeds 0.90, use the charge for 0.90.) Take that charge as the base charge per gram of U-235 in the mixture and 82/12 of that charge as the base charge per gram of U-233 in the mixture. (The ratio of 82/12 is the ratio of charges for highly enriched U-233 and U-235, prior to the deduction given in (2) below.)
- (2) Make the following deduction in dollars per gram of total uranium, depending on the assay of the U-232 isotope. (This deduction will cover estimated handling costs to the AEC when leased uranium is returned after irradiation with an increased U-232 assay.)



Reduced base charges are applicable only in cases in which the AEC has determined that the use of such material will produce technical and economic data of sufficient interest in the AEC program and the lessee has agreed to extend to the AEC access to such data and appropriate patent rights. Under these conditions, the base charge for uranyl nitrate containing uranium enriched in U-233 is \$14 per gram of contained U-233, subject to adjustments of isotopic assays given above except that the ratio of 85/12 shall be replaced by the ratio of 14/12.

In addition to base charges, there are special charges by the AEC for packaging uranium containing U-233 into suitable containers. These charges are not refunded upon return of leased materials.

NUMEC

NEUTRON SOURCE DATA

| | 1 | 2 | 3 | 4 | 5 | 7 | 10 | 20 | 30 | 32.4 | Curies |
|------------------------------|----------------------|----------------------|----------------------|----------------------|----------------------|-------------------|-------------------|-------------------|-------------------|-------------------|------------------------|
| Pu:Be neutron sources | 16 | 32 | 48 | .64 | 80 | 112 | 160 | | | | Grams of Pu |
| Pu half-life: (24,400 years) | 1.8×10^{16} | 3.6×10^{15} | 5.4×10^{14} | 7.2×10^{13} | 9.0×10^{12} | 1.2×10^7 | 1.8×10^7 | | | | Strength Neutrons/sec. |
| Am:Be neutron sources | .3 | .6 | .9 | 1.2 | 1.5 | 2.1 | 3.0 | 6.0 | 9.0 | 10.0 | Grams of Am |
| Am half-life: (458.1 years) | 2.2×10^6 | 4.4×10^6 | 6.6×10^6 | 8.8×10^6 | 1.1×10^7 | 1.5×10^7 | 2.2×10^7 | 4.4×10^7 | 6.6×10^7 | 7.1×10^7 | Strength Neutrons/sec. |

NOTE: A brochure describing NUMEC's complete line of neutron, alpha, beta and gamma sources is available upon request.

AMERICIUM-241

The primary use of americium-241 is in neutron radiation sources. Recent AEC removal of the 10 gram limit on americium will permit filling industrial requirements for americium neutron sources which are now chiefly used for well logging.

Salient characteristics of americium-241 are:

Half-Life: 458.1 years
Specific Activity: 3.24 curies/gram
Alpha Radiation: 5.44 and 5.48 Mev (98%)
Gamma Radiation: 60 Kev (34%)

The AEC base charge for this radioisotope is \$1500 per gram.

NEPTUNIUM-237

The principal use of neptunium-237 is as a component of neutron detection instruments. The AEC base charge for this radioisotope is \$500 per gram.

TYLER STANDARD SCREEN SCALE SIEVES

In the following table the Tyler Standard Screen Scale Sieves Series has been expanded to include intermediate sieves for closer sizing which gives a ratio of the fourth root of two or 1.189 between openings in successive sieves.

Tyler Standard Screen Scale Sieves and U.S. Sieves can be used interchangeably.

| | 30 | 32.4 | Curies | Grams of Pu | Strength Neutrons/sec. | Grams of Am | Strength Neutrons/sec. |
|--|-----|------|--------|-------------|---------------------------|-------------|---------------------------|
| | 9.0 | 10.0 | | | | | |

AEC removal of the 10 tricium neutron sources

pd 5.48 Mev (98%)
ev (34%)

n^os. The

ENERGY CONVERSION FACTORS

| | erg | joule = Watt-sec | Kilowatt-hour | cal |
|----------------------------|-----------------------|-----------------------|-----------------------|-----------------------|
| 1 erg | 1 | 10^{-7} | $2.78 \cdot 10^{-11}$ | $2.39 \cdot 10^{-8}$ |
| 1 joule | 10^7 | 1 | $2.78 \cdot 10^{-7}$ | $2.39 \cdot 10^{-1}$ |
| 1 kilowatt-hour | $3.6 \cdot 10^{13}$ | $3.6 \cdot 10^{10}$ | 1 | $0.86 \cdot 10^6$ |
| 1 cal | $4.19 \cdot 10^7$ | 4.19 | $1.16 \cdot 10^{-6}$ | 1 |
| 1 kgm | $0.98 \cdot 10^8$ | 9.8 | $2.72 \cdot 10^{-6}$ | 2.34 |
| 1 Electronvolt | $1.60 \cdot 10^{-12}$ | $1.60 \cdot 10^{-10}$ | $4.45 \cdot 10^{-26}$ | $3.83 \cdot 10^{-20}$ |
| 1 Mol Electronvolt | $9.65 \cdot 10^{11}$ | $9.65 \cdot 10^4$ | $2.68 \cdot 10^{-2}$ | 23060 |
| 10^{-3} unit atomic mass | $1.49 \cdot 10^{-6}$ | $1.49 \cdot 10^{-13}$ | $4.14 \cdot 10^{-20}$ | $3.56 \cdot 10^{-14}$ |
| 1 g-mass equivalent | $8.99 \cdot 10^{20}$ | $8.99 \cdot 10^{13}$ | $2.50 \cdot 10^7$ | $2.15 \cdot 10^{13}$ |
| 1 Megawatt-day | $8.64 \cdot 10^{17}$ | $8.64 \cdot 10^{10}$ | $2.4 \cdot 10^4$ | $2.06 \cdot 10^{10}$ |

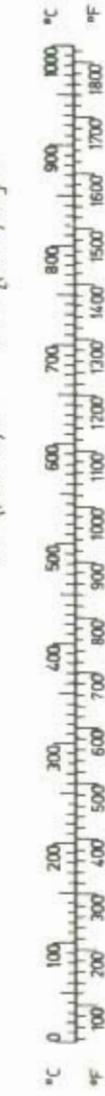
| α | kgm | Electronvolt | 1 MeV Electronvolt | 10^{-3} unit atomic mass | g-mass equivalent | Megawatt-day |
|-----------------------|-----------------------|-----------------------|-----------------------|-------------------------------|------------------------|-----------------------|
| $9 \cdot 10^{-8}$ | $1.02 \cdot 10^{-8}$ | $0.624 \cdot 10^{12}$ | $1.04 \cdot 10^{-12}$ | $0.670 \cdot 10^6$ | $1.113 \cdot 10^2$ | $1.16 \cdot 10^{-18}$ |
| $9 \cdot 10^{-1}$ | $1.02 \cdot 10^{-1}$ | $0.624 \cdot 10^{10}$ | $1.04 \cdot 10^{-10}$ | $0.670 \cdot 10^{13}$ | $1.113 \cdot 10^{-14}$ | $1.16 \cdot 10^{-11}$ |
| $5 \cdot 10^5$ | $3.67 \cdot 10^5$ | $2.25 \cdot 10^{25}$ | 37.3 | $2.41 \cdot 10^{19}$ | $4.01 \cdot 10^{-8}$ | $4.17 \cdot 10^{-5}$ |
| $4.27 \cdot 10^{-1}$ | $2.61 \cdot 10^{19}$ | $4.34 \cdot 10^{-5}$ | $2.81 \cdot 10^{13}$ | $4.66 \cdot 10^{-14}$ | $1.092 \cdot 10^{-13}$ | $4.84 \cdot 10^{-11}$ |
| 1 | $0.612 \cdot 10^{20}$ | $1.02 \cdot 10^{-4}$ | $0.657 \cdot 10^{14}$ | $1.02 \cdot 10^{-10}$ | $1.13 \cdot 10^{-10}$ | |
| $1.63 \cdot 10^{-20}$ | 1 | $1.66 \cdot 10^{-24}$ | $1.074 \cdot 10^{-6}$ | $1.78 \cdot 10^{-33}$ | $1.85 \cdot 10^{-30}$ | |
| $9.84 \cdot 10^3$ | $6.03 \cdot 10^{23}$ | 1 | $6.46 \cdot 10^{17}$ | $1.074 \cdot 10^{-9}$ | $1.11 \cdot 10^{-6}$ | |
| $1.52 \cdot 10^{-14}$ | $0.931 \cdot 10^0$ | $1.55 \cdot 10^{-18}$ | 1 | $1.66 \cdot 10^{-27}$ | $1.73 \cdot 10^{-24}$ | |
| $9.17 \cdot 10^{12}$ | $5.61 \cdot 10^{32}$ | $9.31 \cdot 10^8$ | $6.03 \cdot 10^{26}$ | 1 | $1.04 \cdot 10^3$ | |
| $8.81 \cdot 10^0$ | $5.39 \cdot 10^{29}$ | $8.99 \cdot 10^5$ | $5.79 \cdot 10^{23}$ | $9.61 \cdot 10^{-4}$ | 1 | |

UNIT CONVERSION CHARTS

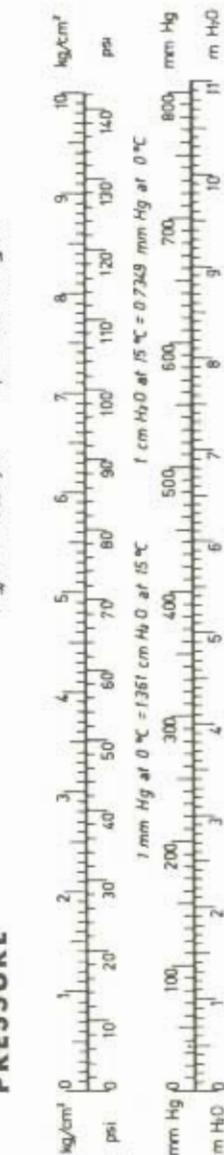
TEMPERATURE

$$t^{\circ}\text{C} = \frac{5}{9}(t^{\circ}\text{F} - 32)$$

$$t^{\circ}\text{F} = \frac{9}{5}t^{\circ}\text{C} + 32$$



PRESSURE

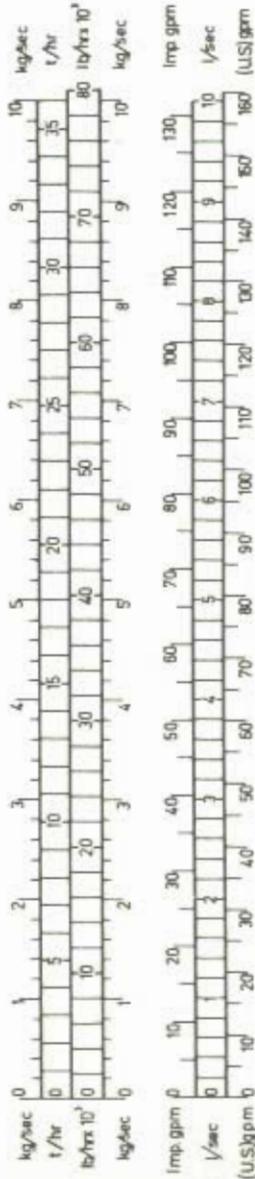


FLOW

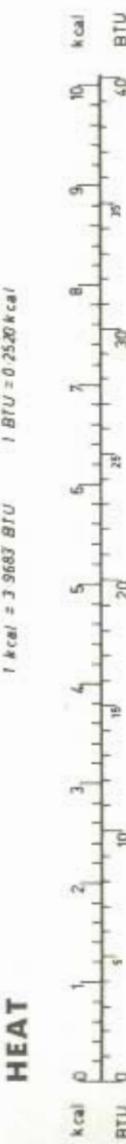
$$t \text{ kg/sec} = 3.6 t \text{ l/hr} = 7925.6 t \text{ lb/sec}$$

$$t \text{ l hr} = 0.2778 \text{ kg/sec} = 2204.6 \text{ lb/sec}$$

$$t \text{ lb/sec} = 1.260 \times 10^5 \text{ kg/sec} = 4.536 \times 10^4 \text{ l/hr}$$

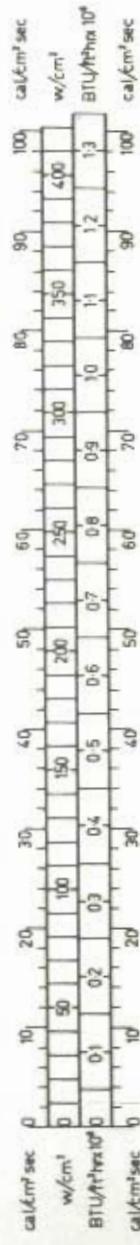


HEAT



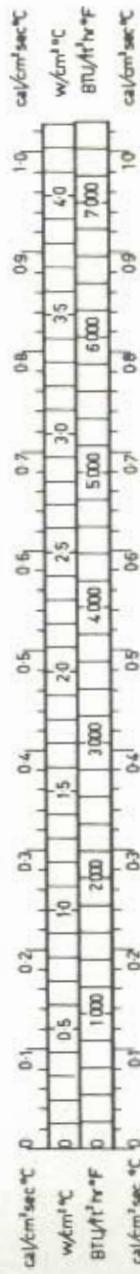
HEAT TRANSFER

$t \text{ cal/cm}^2/\text{sec} = 4.1600 \text{ w/cm}^2 = 1226.3 \text{ BTU/hr}^2/\text{hr}$
 $t \text{ w/cm}^2 = 0.2390 \text{ cal/cm sec} = 3.171 \text{ BTU/hr}^2/\text{hr}$
 $t \text{ BTU/hr}^2/\text{hr} = 0.754 \times 10^{-4} \text{ cal/cm}^2 \text{ sec} = 3.154 \times 10^{-4} \text{ w/cm}^2$



HEAT TRANSFER COEFF.

$t \text{ cal/cm}^2/\text{sec}^\circ\text{C} = 4.1833 \text{ w/cm}^2/\text{C} = 2272.5 \text{ BTU/hr}^2/\text{hr}^\circ\text{C}$
 $t \text{ w/cm}^2/\text{C} = 0.239 \text{ cal/cm}^2/\text{sec}^\circ\text{C} = 2782.2 \text{ BTU/hr}^2/\text{hr}^\circ\text{C}$
 $t \text{ BTU/hr}^2/\text{hr}^\circ\text{C} = 0.753 \times 10^{-4} \text{ cal/cm}^2/\text{sec}^\circ\text{C} = 5.673 \times 10^{-4} \text{ w/cm}^2/\text{C}$



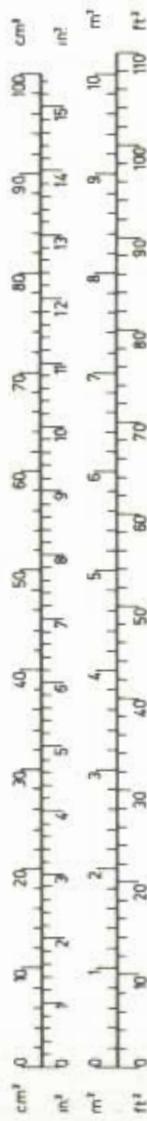
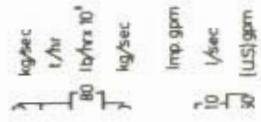
LENGTH

$t \text{ cm} = 0.3937 \text{ in}$
 $t \text{ m} = 3.28083 \text{ ft}$
 $t \text{ km} = 0.62137 \text{ mile}$



AREA

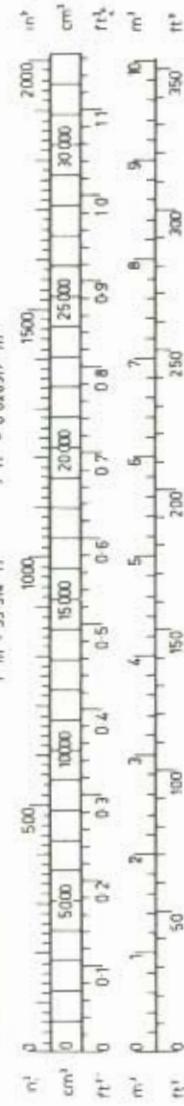
$t \text{ cm}^2 = 0.1550 \text{ in}^2$
 $t \text{ m}^2 = 10.766 \text{ ft}^2$



VOLUME

$$1 \text{ cm}^3 = 0.00003 \text{ m}^3 \quad 1 \text{ m}^3 = 16.000 \text{ cm}^3$$

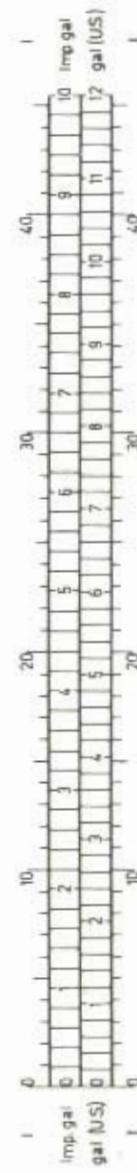
$$1 \text{ m}^3 = 35.314 \text{ ft}^3 \quad 1 \text{ ft}^3 = 0.028317 \text{ m}^3$$

**CAPACITY**

$$1 \text{ l} = 0.21998 \text{ Imp gal} = 0.26417 \text{ gal (US)}$$

$$1 \text{ Imp gal} = 4.5460 \text{ l} = 1.00034 \text{ gal (US)}$$

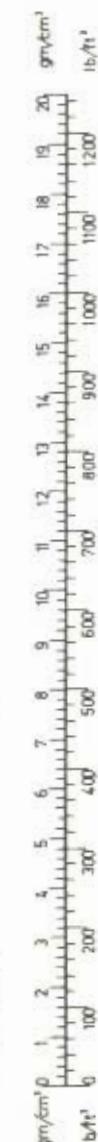
$$1 \text{ gal (US)} = 3.7854 \text{ l} = 0.8327 \text{ Imp gal}$$

**WEIGHT**

$$1 \text{ kg} = 2.2046 \text{ lb} \quad 1 \text{ lb} = 0.4536 \text{ kg}$$

**DENSITY**

$$1 \text{ g/cm}^3 = 62.43 \text{ lb/ft}^3 \quad 1 \text{ lb/ft}^3 = 0.01602 \text{ g/cm}^3$$

**POWER**

$$1 \text{ hp} = 0.7457 \text{ kw} \quad 1 \text{ kw} = 1.341 \text{ hp}$$



AEC OPERATIONS OFFICES

U. S. Atomic Energy Commission
Washington, D. C. 20545
Tel. 301-973-3414

Albuquerque Operations Office

U. S. Atomic Energy Commission
H Street at Pennsylvania
Sandia Base
P. O. Box 5400
Albuquerque, N. Mex. 87115
Tel. 505-264-8211

Chicago Operations Office

U. S. Atomic Energy Commission
9800 South Cass Avenue
Argonne, Ill. 60439
Tel. 312-739-7711

Grand Junction Operations Office

U. S. Atomic Energy Commission
P. O. Box 2567
Grand Junction, Colo. 81502
Tel. 303-242-8621

Idaho Operations Office

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Idaho Falls, Idaho 83401
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Oak Ridge, Tenn. 37831
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Berkeley, Calif. 94704
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Tel. 803-642-7211

Brookhaven Office

U. S. Atomic Energy Commission
Upton, L. I., New York 11973
Tel. 516-924-6262

Pittsburgh Naval Reactors Office

U. S. Atomic Energy Commission
P. O. Box 109
West Mifflin, Pa. 15122
Tel. 412-462-5000

Schenectady Naval Reactors Office

U. S. Atomic Energy Commission
P. O. Box 1069
Schenectady, N. Y. 12301
Tel. 518-393-6611

TUESDAY

MONDAY

SUNDAY

| | | | | |
|--|--|--|--|--|
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |

JANUARY

1966

DECEMBER

| S | M | T | W | T | F | S |
|----|----|----|----|----|----|----|
| | | 1 | 2 | 3 | 4 | |
| 5 | 6 | 7 | 8 | 9 | 10 | 11 |
| 12 | 13 | 14 | 15 | 16 | 17 | 18 |
| 19 | 20 | 21 | 22 | 23 | 24 | 25 |
| 26 | 27 | 28 | 29 | 30 | 31 | |

11

10

9

18

17

16

11

FEBRUARY

| S | M | T | W | T | F | S |
|----|----|----|----|----|----|----|
| | | 1 | 2 | 3 | 4 | 5 |
| 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 13 | 14 | 15 | 16 | 17 | 18 | 19 |
| 20 | 21 | 22 | 23 | 24 | 25 | 26 |
| 27 | 28 | | | | | |

25

24

30

25

31

NUMEC

- Bulk Uranium Fuel Materials
 - Refractory Metal Powder
 - Nuclear Moisture Density Meters
 - Metallic and Ceramic Coatings
 - Equipment Decontamination and Renovation

* CABLE: NUMEC-APOLLO

SUNDAY

MONDAY

TUESDAY

FEBRUARY

1966

JANUARY
S M T W T F S

| | | | | | | |
|----|----|----|----|----|----|----|
| 9 | 10 | 11 | 12 | 13 | 14 | 15 |
| 16 | 17 | 18 | 19 | 20 | 21 | 22 |
| 23 | 24 | 25 | 26 | 27 | 28 | 29 |
| 30 | | | | | | |

| MARCH | | | | | | |
|-------|----|----|----|----|----|----|
| S | M | T | W | T | F | S |
| | | 1 | 2 | 3 | 4 | 5 |
| 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 13 | 14 | 15 | 16 | 17 | 18 | 19 |
| 20 | 21 | 22 | 23 | 24 | 25 | 26 |
| | | 27 | 28 | 29 | 30 | 31 |

VALENTINE DAY

WASHINGTON'S BIRTHDAY

28

27

NUMEC

SATURDAY

FRIDAY

THURSDAY

WEDNESDAY

TUESDAY

MONDAY

1

8

15

7

14

2

10

16

3

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17

4

11

18

5

12

19

LINCOLN'S BIRTHDAY

- Bulk Plutonium Fuel Materials

- Zirconium, Zircaloy, and Hafnium Metal Powders

- Cathodic Vacuum Etchers

- Controlled Porosity Shape

- Gamma Irradiators

ASH WEDNESDAY

WASHINGTON'S BIRTHDAY

28

26

24

23

25

19

18

17

16

14

15

NUMEC



| Y | TUESDAY | WEDNESDAY | THURSDAY | FRIDAY | SATURDAY |
|----|---------|-----------|----------|--------|----------|
| | 1 | 2 | 3 | 4 | 5 |
| 7 | 8 | 9 | 10 | 11 | 12 |
| 14 | 15 | 16 | 17 | 18 | 19 |
| 21 | 22 | 23 | 24 | 25 | 26 |
| 28 | 29 | 30 | 31 | | |

- Nuclear Fuel Spherical Particles — U, Pu, Th

- Plutonium Scrap Recovery
- Alpha, Beta, and Gamma Sources

- Control Rod Materials
- Glove Box Installations

AY

WEDNESDAY

FRIDAY

SATURDAY

NUMEC



- Fabricated Nuclear Fuels—
U, Pu, Th

PASSOVER—FIRST DAY

11 12

18 19

25 26

PASSOVER—SECOND DAY

13

20 21

27

GOOD FRIDAY

14

22 23

28

16

15

16

29 30

- Hafnium and Zirconium
Foil, Rod and Wire

- Thermionic Convertors

- Instrumental and Wet
Chemical Analyses

NUMEC

| | | | | | |
|----|----|----|----|----|----|
| 2 | 3 | 4 | 5 | 6 | 7 |
| 9 | 10 | 11 | 12 | 13 | 14 |
| 16 | 17 | 18 | 19 | 20 | 21 |
| 23 | 24 | 25 | 26 | 27 | 28 |
| 30 | 31 | | | | |

• Nuclear Fuel Rods —
U, Pu, Th

• Brazing Alloys — Zr-Be,
Ni-Ti, Ni-Nb

• Derivative Polarographic
Instruments

• Isotopic Heat Sources

• Corrosion Testing

SUNDAY MONDAY TUESDAY

JUNE

1966

MAY

| S | M | T | W | T | F | S |
|----|----|----|----|----|----|----|
| 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 8 | 9 | 10 | 11 | 12 | 13 | 14 |
| 15 | 16 | 17 | 18 | 19 | 20 | 21 |
| 22 | 23 | 24 | 25 | 26 | 27 | 28 |
| 29 | 30 | 31 | | | | |

JULY

| S | M | T | W | T | F | S |
|----|----|----|----|----|----|----|
| | | | | | 1 | 2 |
| 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 10 | 11 | 12 | 13 | 14 | 15 | 16 |
| 17 | 18 | 19 | 20 | 21 | 22 | 23 |
| 24 | 25 | 26 | 27 | 28 | 29 | 30 |
| 31 | | | | | | |

5 6 7

12 13 14

19 20 21

27 28

FLAG DAY

NUMEC



| DAY | TUESDAY | WEDNESDAY | THURSDAY | FRIDAY | SATURDAY |
|-----|---------|-----------|----------|--------|----------|
| | | 1 | 2 | 3 | 4 |
| | 6 | 7 | 8 | 9 | 10 |
| | | | | | 11 |
| | | | | | 12 |
| | | | | | 13 |
| | | | | | 14 |
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| | | | | | 30 |

- U-233 Processing and Fabrication

- Burnable Poison Materials

- Particle Crush Strength Testers

- Thermoelectric Generators

- Radioprocess Facility Design and Construction

JULY

1966

| | | | |
|----|----|------------------|--|
| | | | |
| 3 | 4 | 5 | |
| | | INDEPENDENCE DAY | |
| 10 | 11 | 12 | |
| 17 | 18 | 19 | |
| 24 | 25 | 26 | |
| 31 | | | |

JUNE 1970

| | 1 | 2 | 3 | 4 |
|----|----|----|----|----|
| 5 | 6 | 7 | 8 | 9 |
| 12 | 13 | 14 | 15 | 16 |
| 19 | 20 | 21 | 22 | 23 |
| 26 | 27 | 28 | 29 | 30 |

AUGUST

| S | M | T | W | T | F | S |
|----|----|----|----|----|----|----|
| 1 | 2 | 3 | 4 | 5 | 6 | |
| 7 | 8 | 9 | 10 | 11 | 12 | 13 |
| 14 | 15 | 16 | 17 | 18 | 19 | 20 |
| 21 | 22 | 23 | 24 | 25 | 26 | 27 |
| 28 | 29 | 30 | 31 | | | |

NUMEC

| WEDNESDAY | THURSDAY | FRIDAY | SATURDAY |
|-----------|----------|--------|----------|
| | | 1 | 2 |
| 6 | 7 | 8 | 9 |
| | | | |
| 13 | 14 | 15 | 16 |
| | | | |
| 20 | 21 | 22 | 23 |
| | | | |
| 27 | 28 | 29 | 30 |

CONTINUOUS ADDITION

| SUNDAY | MONDAY | TUESDAY |
|--------|--------|---------|
| | 1 | 2 |
| | 7 | 8 |
| | 14 | 15 |
| | 21 | 22 |
| | 28 | 29 |
| | | 30 |

AUGUST
1966

NUMEC



- Nuclear Fuel Research and Development

| DAY | TUESDAY | WEDNESDAY | THURSDAY | FRIDAY | SATURDAY |
|-----|---------|-----------|----------|--------|----------|
| 1 | | | | 4 | 5 |
| 8 | 9 | 10 | 11 | 12 | 13 |
| 15 | 16 | 17 | 18 | 19 | 20 |
| 22 | 23 | 24 | 25 | 26 | 27 |
| 29 | 30 | 31 | | | |
| | | | | | |

- Nuclear Fuel Research and Development
- Refractory Metal Alloy Shapes
- Automatic Weight, Density, Dimension Inspection Device
- Fabricated Plutonium Metal Fuel Plates and Elements
- Metallographic Investigations

1 MAY

2

9

16

23

30

SATURDAY

FRIDAY

THURSDAY

WEDNESDAY

TUESDAY

SUNDAY MONDAY TUESDAY

SEPTEMBER

1966

4

5

6

LABOR DAY

11

12

13

AUGUST

| S | M | T | W | T | F | S |
|----|----|----|----|----|----|----|
| | 1 | 2 | 3 | 4 | 5 | 6 |
| 7 | 8 | 9 | 10 | 11 | 12 | 13 |
| 14 | 15 | 16 | 17 | 18 | 19 | 20 |
| 21 | 22 | 23 | 24 | 25 | 26 | 27 |
| 28 | 29 | 30 | 31 | | | |

18

19

20

OCTOBER

| S | M | T | W | T | F | S |
|----|----|----|----|----|----|----|
| | 2 | 3 | 4 | 5 | 6 | 7 |
| 9 | 10 | 11 | 12 | 13 | 14 | 15 |
| 16 | 17 | 18 | 19 | 20 | 21 | 22 |
| 23 | 24 | 25 | 26 | 27 | 28 | 29 |
| 30 | 31 | | | | | |

25

26

27

NUMEC

WEDNESDAY

FRIDAY

THURSDAY

SATURDAY



6

5

12

13

19

20

26

- Specialty Shapes — Enriched and Depleted Uranium

- Constant Potential Coulometric Titrators

- Irradiated Fuel Evaluations

- Replacement Gamma Irradiator Sources

- Vapor Deposited Coating and Cementation

JEWISH NEW YEAR—1st DAY

17

JEWISH NEW YEAR—2nd DAY

16

23

24

25

26

27

28

29

30

YOM KIPPUR

TUESDAY
MONDAY
SUNDAY

OCTOBER

1966

2 3 4

9 10 11

SEPTEMBER

| S | M | T | W | T | F | S |
|----|----|----|----|----|----|----|
| | | | | 1 | 2 | 3 |
| 4 | 5 | 6 | 7 | 8 | 9 | 10 |
| 11 | 12 | 13 | 14 | 15 | 16 | 17 |
| 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 25 | 26 | 27 | 28 | 29 | 30 | |

16 17 18

NOVEMBER

| S | M | T | W | T | F | S |
|----|----|----|----|----|----|----|
| | | | | 1 | 2 | 3 |
| 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 13 | 14 | 15 | 16 | 17 | 18 | 19 |
| 20 | 21 | 22 | 23 | 24 | 25 | 26 |
| 27 | 28 | 29 | 30 | | | |

23 30 24 31 25

HALLOWEEN

NOVEMBER DECEMBER JANUARY

NUMEC



| TUESDAY | WEDNESDAY | THURSDAY | FRIDAY | SATURDAY |
|---------|-----------|----------|--------|----------|
| | | | | 1 |
| 3 | 4 | | | |
| 10 | 11 | | | |
| 17 | 18 | | | |
| 24 | 25 | | | |
| 31 | | | | |

• Enriched Uranium Metal
 • Fuel Plates and Elements
 • Controlled Porosity Shapes
 • Electronic Weight Balances
 • Nuclear Fuel Material
 • Analyses



| | | | | |
|----|----|--|--|--|
| | | | | |
| 3 | 4 | | | |
| 10 | 11 | | | |
| 17 | 18 | | | |

• RADIUM - MIRRORS - AND
 • TELEPHONE: 412-479-RATT - TWX: A12 ECR 2419

| | | | |
|---------|---|---|---|
| SUNDAY | | | |
| MONDAY | | | |
| TUESDAY | 1 | | |
| | 6 | 7 | 8 |

ELECTION DAY

NOVEMBER

1966

OCTOBER

| S | M | T | W | T | F | S |
|---|----|----|----|----|----|----|
| | 2 | 3 | 4 | 5 | 6 | 7 |
| | 9 | 10 | 11 | 12 | 13 | 14 |
| | 16 | 17 | 18 | 19 | 20 | 21 |
| | 23 | 24 | 25 | 26 | 27 | 28 |
| | 30 | 31 | | | | |

DECEMBER

| S | M | T | W | T | F | S |
|---|----|----|----|----|----|----|
| | 4 | 5 | 6 | 7 | 8 | 9 |
| | 11 | 12 | 13 | 14 | 15 | 16 |
| | 18 | 19 | 20 | 21 | 22 | 23 |
| | 25 | 26 | 27 | 28 | 29 | 30 |
| | | | | | | |

NUMEC



- Reactive Metal Alloy Shapes

- Powder Characterizations

- Neutron Sources — Pu-Be, Am-Be, Po-Be

- Cathodic Vacuum Etchers and Evaporators

- Rolling, Extrusion, and Swaging Services

| | TUESDAY | WEDNESDAY | THURSDAY | FRIDAY | SATURDAY |
|----|---------|-----------|----------|---------------|----------|
| | 1 | 2 | 3 | 4 | 5 |
| 7 | 8 | 9 | 10 | 11 | 12 |
| | | | | VETERANS' DAY | |
| 14 | 15 | 16 | 17 | 18 | 19 |
| 21 | 22 | 23 | 24 | 25 | 26 |
| 28 | 29 | 30 | | THANKSGIVING | |

| | | | | | |
|-----|---|---|----|----|----|
| JAN | 1 | 8 | 15 | 22 | 29 |
| | | | | | |
| | | | | | |
| | | | | | |

| SUNDAY | MONDAY | TUESDAY | WEDNESDAY | THURSDAY | FRIDAY | SATURDAY |
|--------|--------|---------|-----------|----------|--------|-----------|
| | | | | | | |
| | 4 | 5 | 6 | | | |
| | | | 11 | 12 | 13 | |
| | | | | | | |
| | | | 18 | 19 | 20 | |
| | | | | | | |
| | | | 25 | 26 | 27 | CHRISTMAS |

DECEMBER

1966

| NOVEMBER | | | | | |
|----------|---|---|----|----|----|
| S | M | T | W | T | F |
| | | | 1 | 2 | 3 |
| | | | 9 | 10 | 11 |
| | | | 16 | 17 | 18 |
| | | | 23 | 24 | 25 |
| | | | 29 | 30 | |

| | JANUARY | | | | | |
|----|---------|----|----|----|----|----|
| S | M | T | W | T | F | S |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| 8 | 9 | 10 | 11 | 12 | 13 | 14 |
| 15 | 16 | 17 | 18 | 19 | 20 | 21 |
| 22 | 23 | 24 | 25 | 26 | 27 | 28 |
| | 29 | 30 | 31 | | | |

CHRISTMAS

NUMEC



| WEDNESDAY | THURSDAY | FRIDAY | SATURDAY |
|-----------|----------|--------|----------|
| | 1 | 2 | 3 |
| 7 | 8 | 9 | 10 |
| 14 | 15 | 16 | 17 |
| 21 | 22 | 23 | 24 |
| 28 | 29 | 30 | 31 |

CABLE: NUMEC-APOLLO

TELEPHONE: 412-472-8411 * TWX: 412-204-7000

| | | | |
|---------|---|---|---|
| SUNDAY | 1 | 2 | 3 |
| MONDAY | | | |
| TUESDAY | | | |
| | | | |
| | | | |

JANUARY

1967

DECEMBER

| S | M | T | W | T | F | S |
|----|----|----|----|----|----|----|
| | | | 1 | 2 | 3 | |
| 4 | 5 | 6 | 7 | 8 | 9 | 10 |
| 11 | 12 | 13 | 14 | 15 | 16 | 17 |
| 18 | 19 | 20 | 21 | 22 | 23 | 24 |
| 25 | 26 | 27 | 28 | 29 | 30 | 31 |

15 16 17

FEBRUARY

| S | M | T | W | T | F | S |
|----|----|----|----|----|----|----|
| | | | 1 | 2 | 3 | 4 |
| 5 | 6 | 7 | 8 | 9 | 10 | 11 |
| 12 | 13 | 14 | 15 | 16 | 17 | 18 |
| 19 | 20 | 21 | 22 | 23 | 24 | 25 |
| 26 | 27 | 28 | | | | |

22 23 24

29 30 31

NUMEC



• Spherical Metal Powders

- Remotized Cathodic Vacuum Etchers

- Radioisotope Source Encapsulation

- Facility Management and Operation

- Materials Research and Development

| MONDAY | TUESDAY | WEDNESDAY | THURSDAY | FRIDAY | SATURDAY |
|--------|---------|-----------|----------|--------|----------|
| | | | | 5 | 6 |
| 2 | 3 | 4 | | | 7 |
| 9 | 10 | 11 | 12 | 13 | 14 |
| 16 | 17 | 18 | 19 | 20 | 21 |
| 23 | 24 | 25 | 26 | 27 | 28 |
| 30 | 31 | | | | |

| | | | | | |
|----|----|----|----|----|----|
| | | | | | |
| 2 | 3 | 4 | 5 | 6 | 7 |
| 9 | 10 | 11 | 12 | 13 | 14 |
| 16 | 17 | 18 | 19 | 20 | 21 |
| 23 | 24 | 25 | 26 | 27 | 28 |
| 30 | 31 | | | | |

1965

| JANUARY 1965 | | | | | | JULY 1965 | | | | | |
|--------------|----|----|----|----|----|-----------|----|----|----|----|----|
| S | M | T | W | T | F | S | M | T | W | T | F |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 |
| 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 |
| 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 1 | 2 |
| 29 | 30 | 31 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |

| FEBRUARY 1965 | | | | | | AUGUST 1965 | | | | | |
|---------------|----|----|----|----|----|-------------|----|----|----|----|----|
| S | M | T | W | T | F | S | M | T | W | T | F |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 |
| 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 |
| 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 1 |
| 28 | 29 | 30 | 31 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |

| MARCH 1965 | | | | | | SEPTEMBER 1965 | | | | | |
|------------|----|----|----|----|----|----------------|----|----|----|----|----|
| S | M | T | W | T | F | S | M | T | W | T | F |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 |
| 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 |
| 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 1 |
| 28 | 29 | 30 | 31 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |

| APRIL 1965 | | | | | | OCTOBER 1965 | | | | | |
|------------|----|----|----|----|----|--------------|----|----|----|----|----|
| S | M | T | W | T | F | S | M | T | W | T | F |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 |
| 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 |
| 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 1 | 2 |
| 29 | 30 | 31 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |

| MAY 1965 | | | | | | NOVEMBER 1965 | | | | | |
|----------|----|----|----|----|----|---------------|----|----|----|----|----|
| S | M | T | W | T | F | S | M | T | W | T | F |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 |
| 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 |
| 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 |
| 25 | 26 | 27 | 28 | 29 | 30 | 1 | 2 | 3 | 4 | 5 | 6 |

| JUNE 1965 | | | | | | DECEMBER 1965 | | | | | |
|-----------|----|----|----|----|----|---------------|----|----|----|----|----|
| S | M | T | W | T | F | S | M | T | W | T | F |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 |
| 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 |
| 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 1 | 2 |
| 30 | 31 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |

| JULY 1965 | | | | | | JULY 1966 | | | | | |
|-----------|----|----|----|----|----|-----------|----|----|----|----|----|
| S | M | T | W | T | F | S | M | T | W | T | F |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 |
| 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 1 | 2 |
| 29 | 30 | 31 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |

| AUGUST 1965 | | | | | | AUGUST 1966 | | | | | |
|-------------|----|----|----|----|----|-------------|----|----|----|----|----|
| S | M | T | W | T | F | S | M | T | W | T | F |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 |
| 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 1 | 2 |
| 29 | 30 | 31 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |

| SEPTEMBER 1965 | | | | | | SEPTEMBER 1966 | | | | | |
|----------------|----|----|----|----|----|----------------|----|----|----|----|----|
| S | M | T | W | T | F | S | M | T | W | T | F |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 |
| 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 1 | 2 |
| 29 | 30 | 31 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |

| OCTOBER 1965 | | | | | | OCTOBER 1966 | | | | | |
|--------------|----|----|----|----|----|--------------|----|----|----|----|----|
| S | M | T | W | T | F | S | M | T | W | T | F |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 |
| 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 1 | 2 |
| 29 | 30 | 31 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |

| NOVEMBER 1965 | | | | | | NOVEMBER 1966 | | | | | |
|---------------|----|----|----|----|----|---------------|----|----|----|----|----|
| S | M | T | W | T | F | S | M | T | W | T | F |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 |
| 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 1 | 2 |
| 29 | 30 | 31 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |

| DECEMBER 1965 | | | | | | DECEMBER 1966 | | | | | |
|---------------|----|----|----|----|----|---------------|----|----|----|----|----|
| S | M | T | W | T | F | S | M | T | W | T | F |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 |
| 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 1 | 2 |
| 29 | 30 | 31 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |

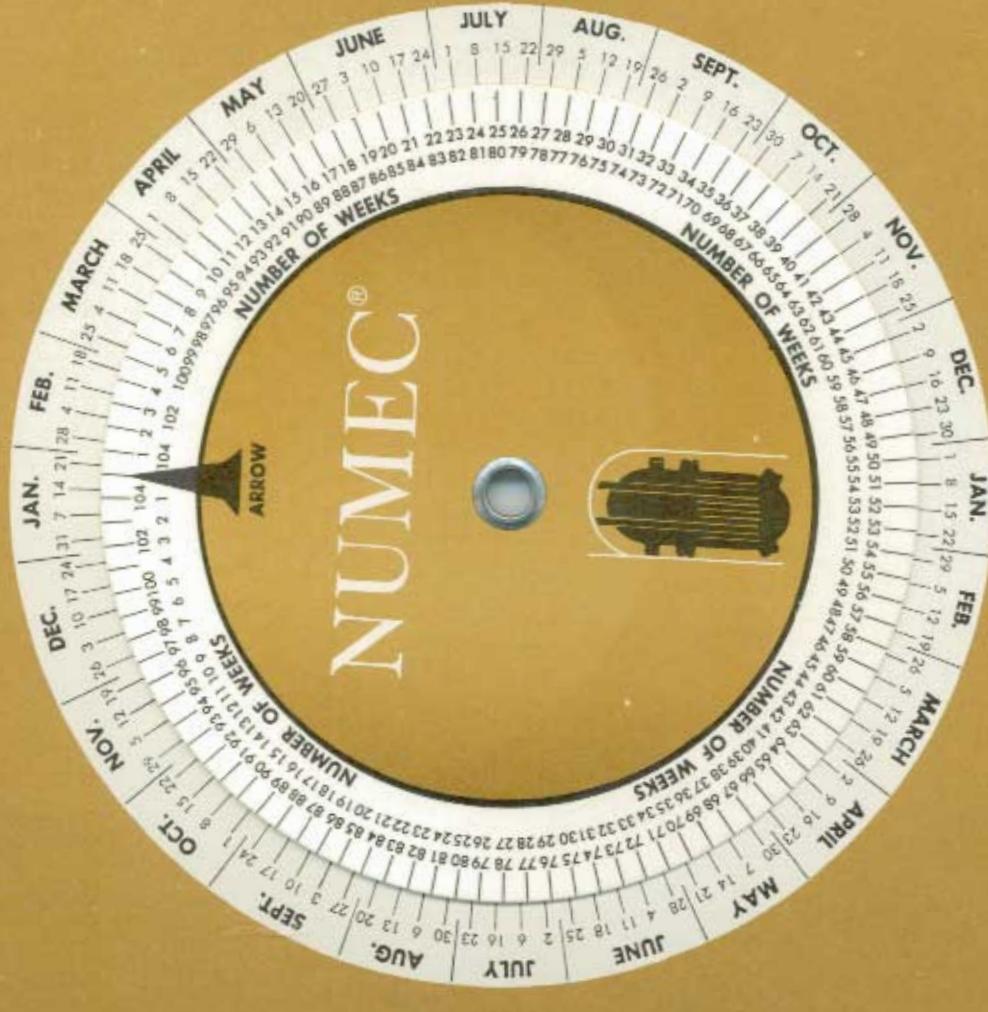
1966

| JANUARY 1966 | | | | | | JULY 1 | | | | | |
| --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |

DATE CALCULATOR

1022367597
NATIONAL ARCHIVAL LIBRARY

1967



DUE DATE
1967

| JULY 1967 | | AUGUST 1967 | |
|-----------|----|-------------|----|
| W | T | S | M |
| 4 | 5 | 6 | 7 |
| 11 | 12 | 13 | 14 |
| 18 | 19 | 20 | 21 |
| 25 | 26 | 27 | 28 |
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| AUGUST 1967 | | SEPTEMBER 1967 | |
|-------------|----|----------------|----|
| W | T | S | M |
| 1 | 2 | 3 | 4 |
| 8 | 9 | 10 | 11 |
| 15 | 16 | 17 | 18 |
| 22 | 23 | 24 | 25 |
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| SEPTEMBER 1967 | | OCTOBER 1967 | |
|----------------|----|--------------|----|
| W | T | S | M |
| 1 | 2 | 3 | 4 |
| 8 | 9 | 10 | 11 |
| 15 | 16 | 17 | 18 |
| 22 | 23 | 24 | 25 |
| 29 | 30 | 31 | |

| OCTOBER 1967 | | NOVEMBER 1967 | |
|--------------|----|---------------|----|
| W | T | S | M |
| 1 | 2 | 3 | 4 |
| 8 | 9 | 10 | 11 |
| 15 | 16 | 17 | 18 |
| 22 | 23 | 24 | 25 |
| 29 | 30 | 31 | |

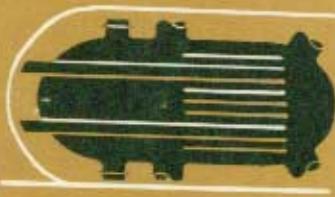
| NOVEMBER 1967 | | DECEMBER 1967 | |
|---------------|----|---------------|----|
| W | T | S | M |
| 1 | 2 | 3 | 4 |
| 8 | 9 | 10 | 11 |
| 15 | 16 | 17 | 18 |
| 22 | 23 | 24 | 25 |
| 29 | 30 | 31 | |

- Completion date based on desired beginning date:**
- Set arrow opposite beginning date.
 - Read clockwise on number of weeks scale to the time cycle required.
 - Read off completion date.
- Beginning date based on desired completion date:**
- Set arrow opposite desired completion date.
 - Read counterclockwise on the number of weeks to the time cycle required.
 - Read off the necessary beginning date.



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16
23



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